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(54) **PARACORPOREAL RESPIRATORY ASSIST LUNG**

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See application file for complete search history.

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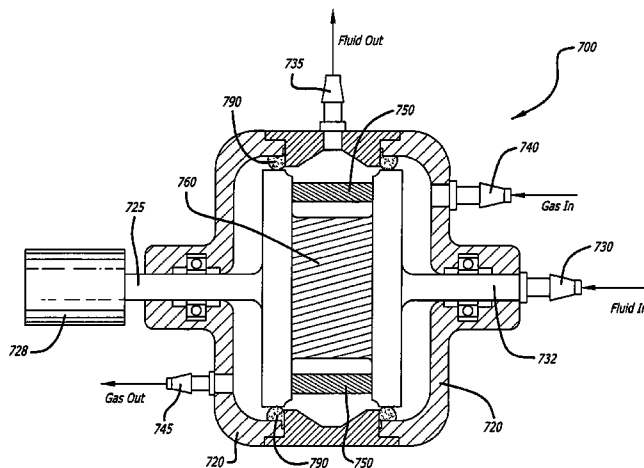
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(57) **ABSTRACT**

A paracorporeal respiratory assist lung is configured with an annular cylindrical hollow fiber membrane (fiber bundle) that is rotated at rapidly varying speeds. Fluid (for example, blood) is introduced to the center of the device and is passed radially through the fiber bundle. The bundle is rotated at rapidly changing velocities with a rotational actuator (for example, a motor or magnetic coupling). The rotation of the fiber bundle provides centrifugal kinetic energy to the fluid giving the device pumping capabilities and may create Taylor vortices to increase mass transfer. Rotation of the fiber bundle increases the relative velocity between the fluid and the hollow fibers and increases the mass transfer. The porosity of the fiber bundle may be varied to enhance gas exchange with the blood. Alternatively, a rotating core may be used with a stationary fiber bundle.

5 Claims, 30 Drawing Sheets



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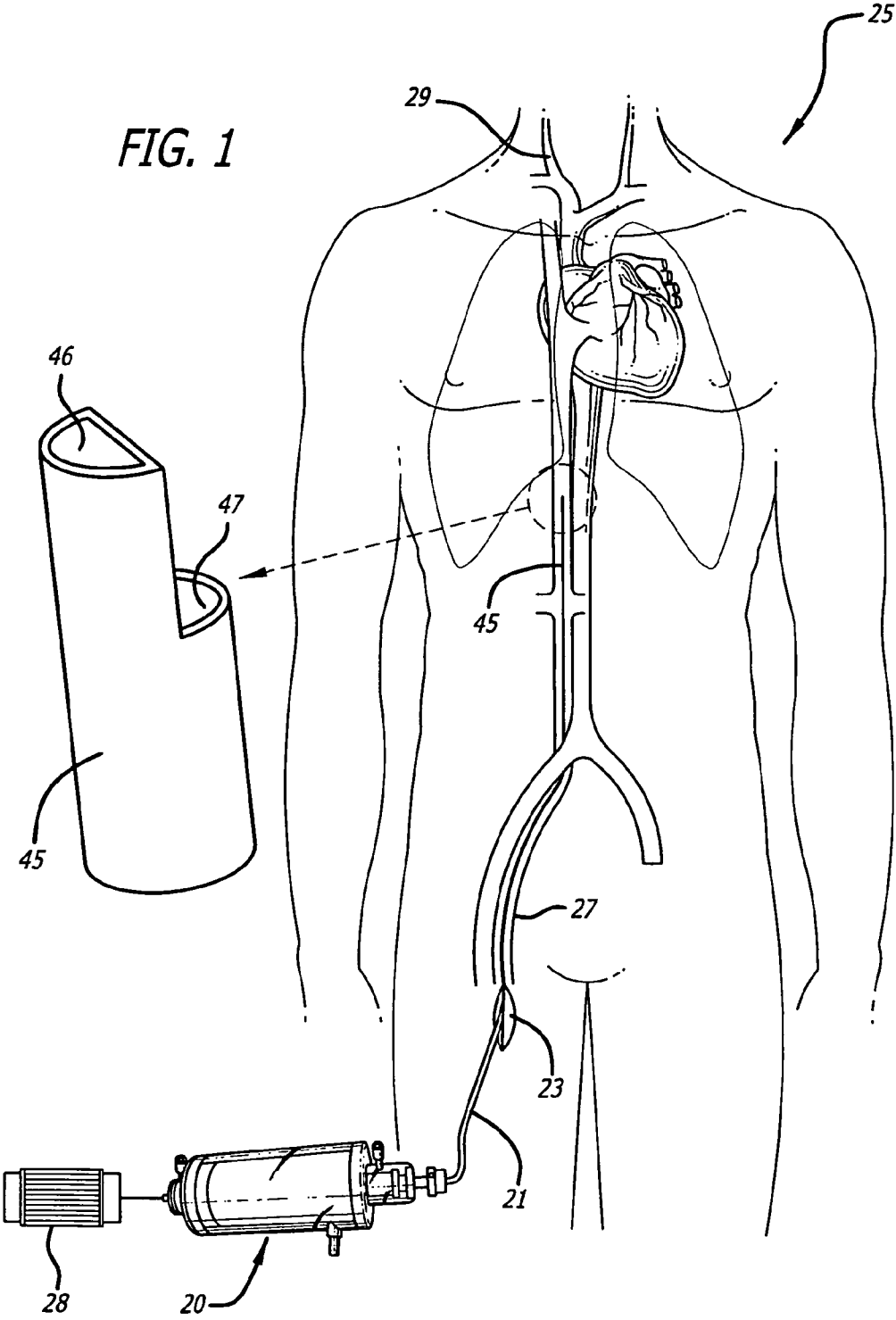
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FIG. 1



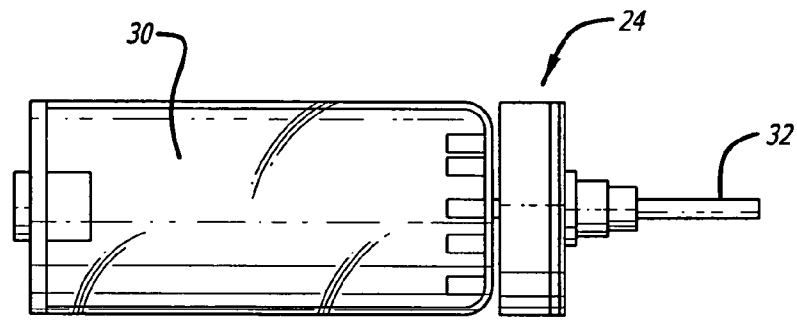
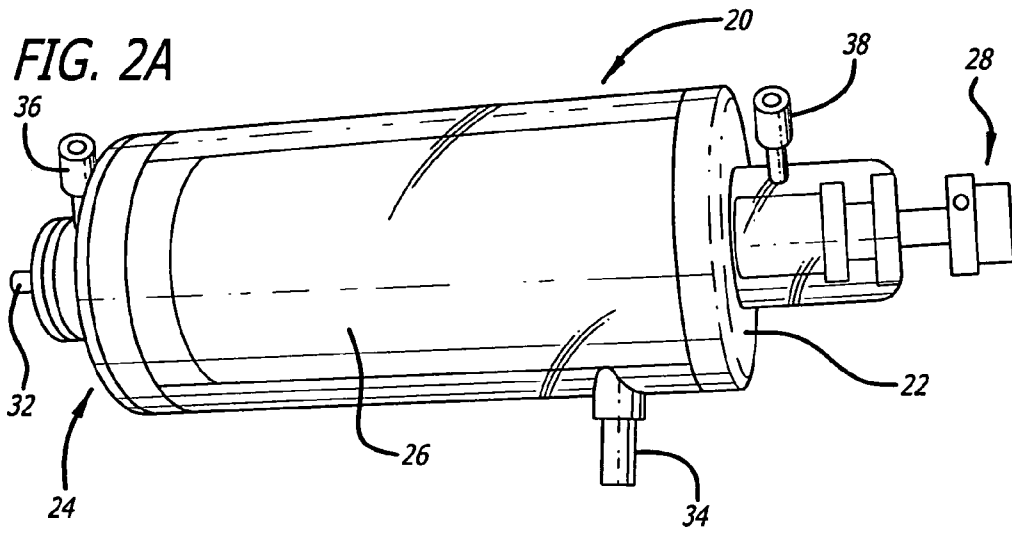


FIG. 2B

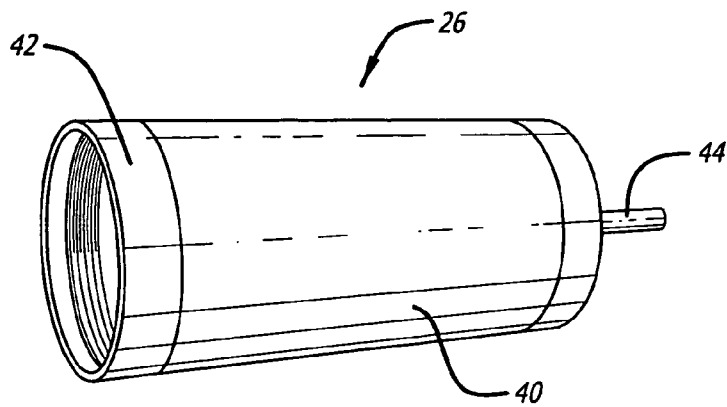
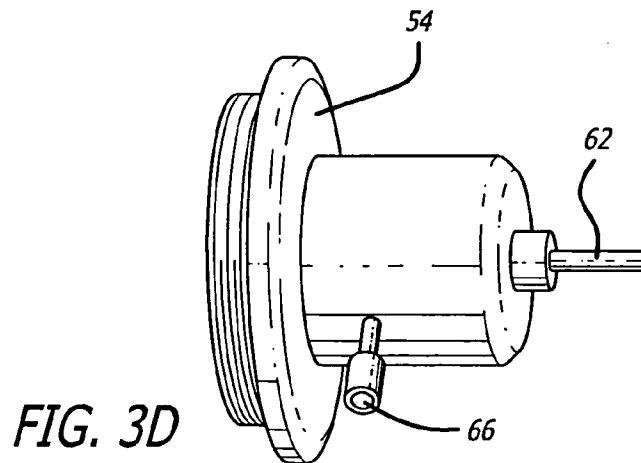
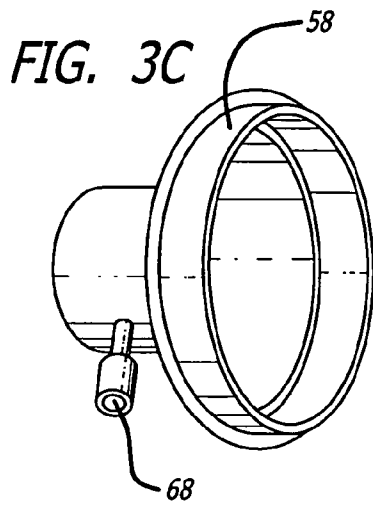
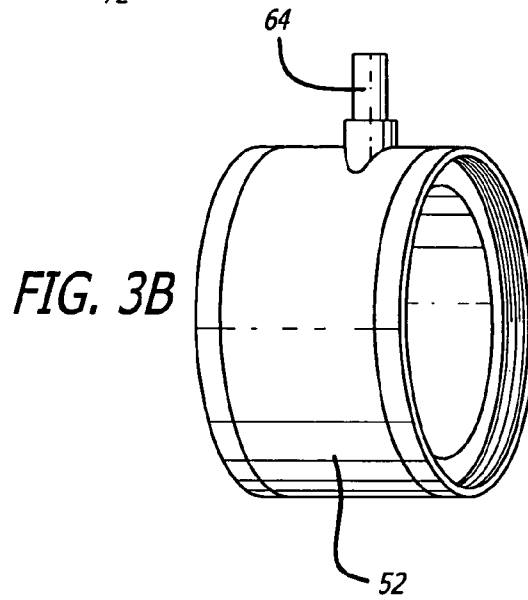
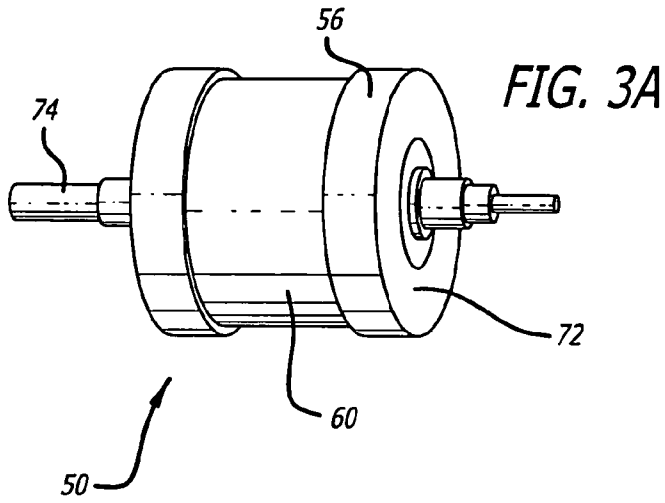
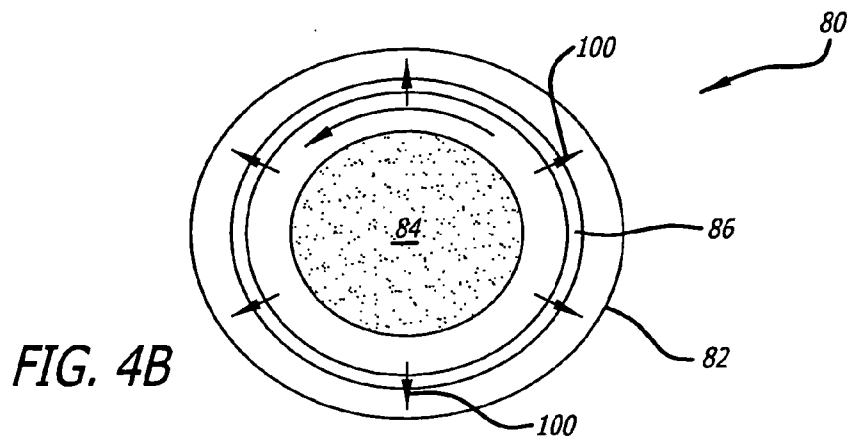
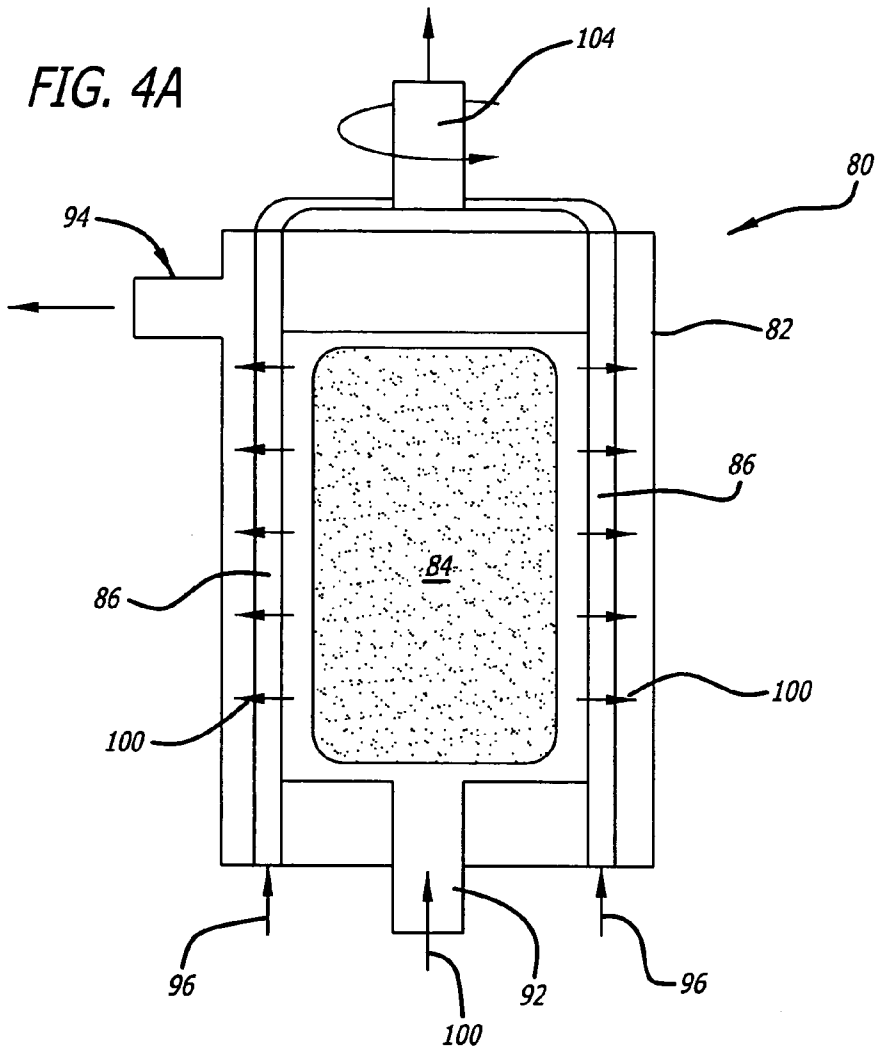
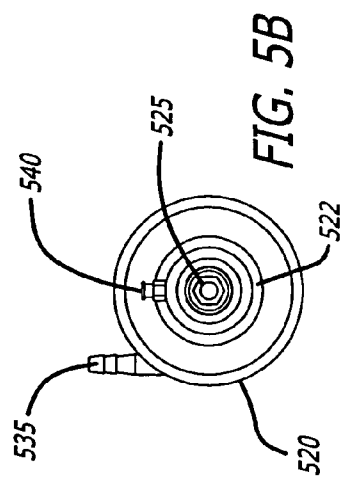
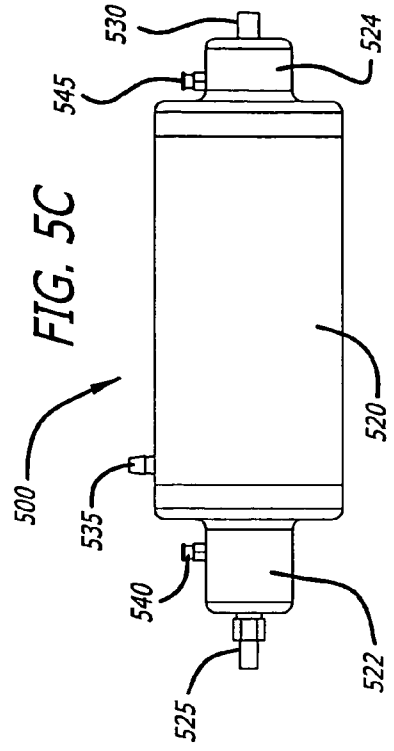
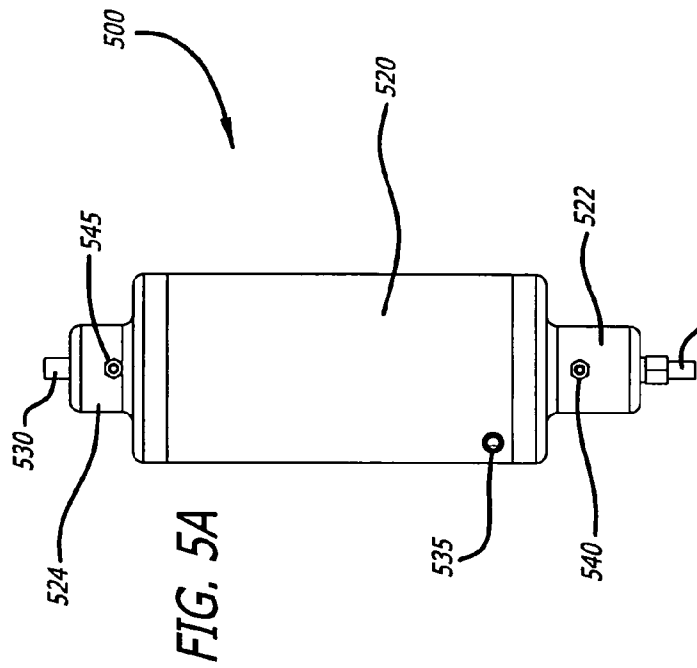


FIG. 2C







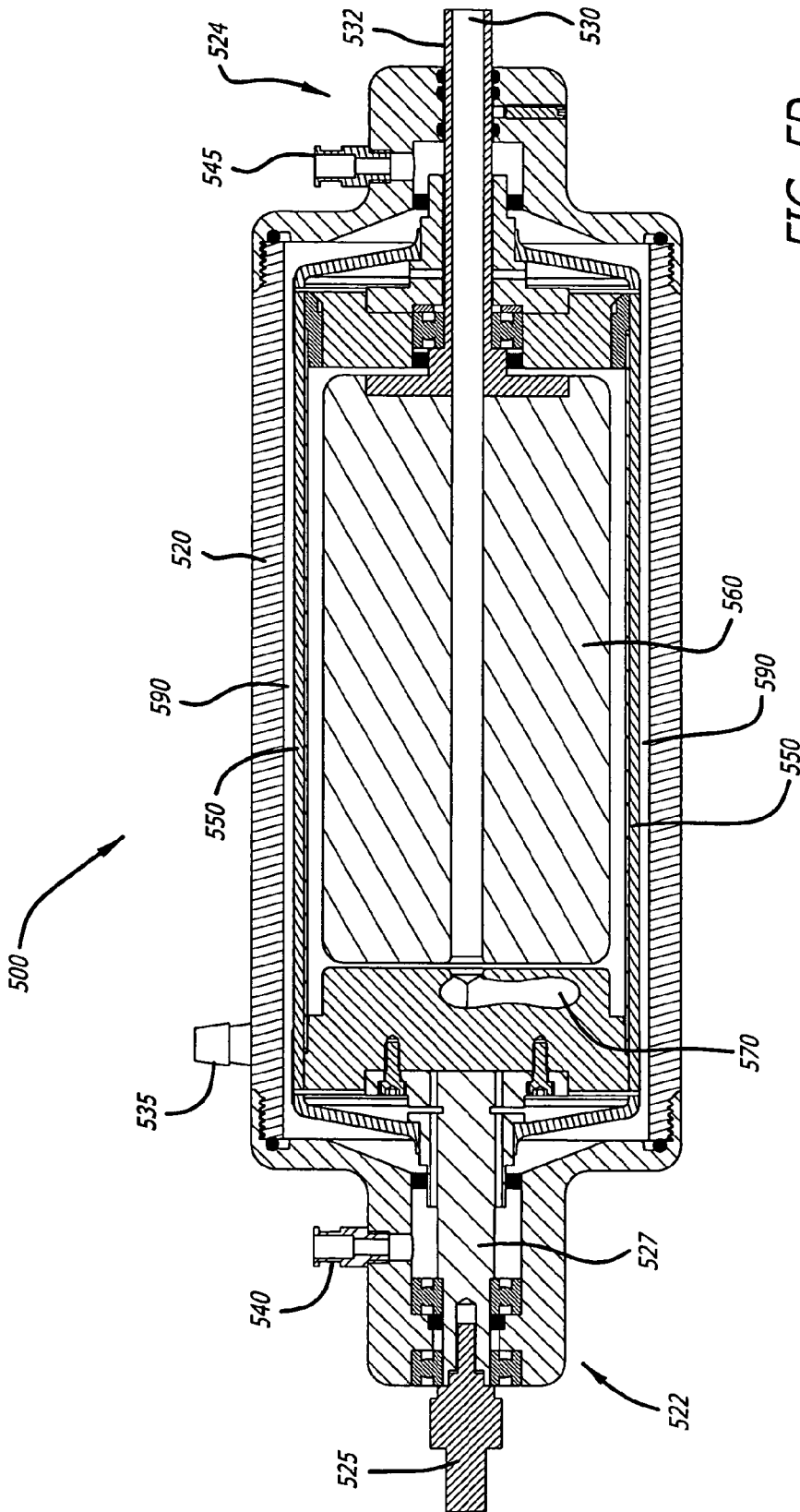
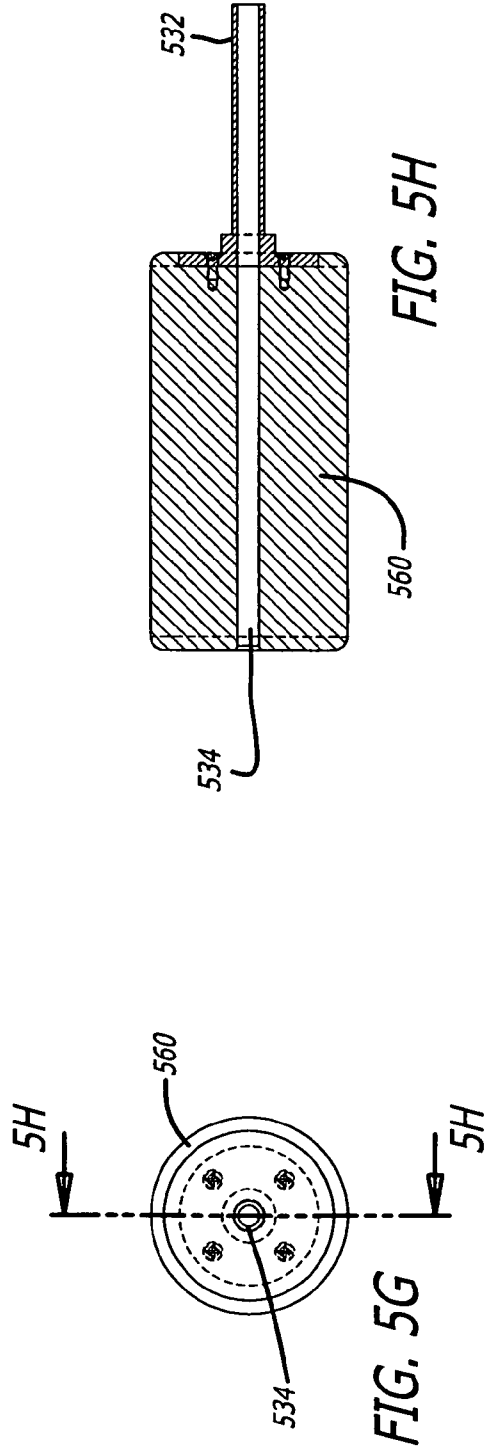
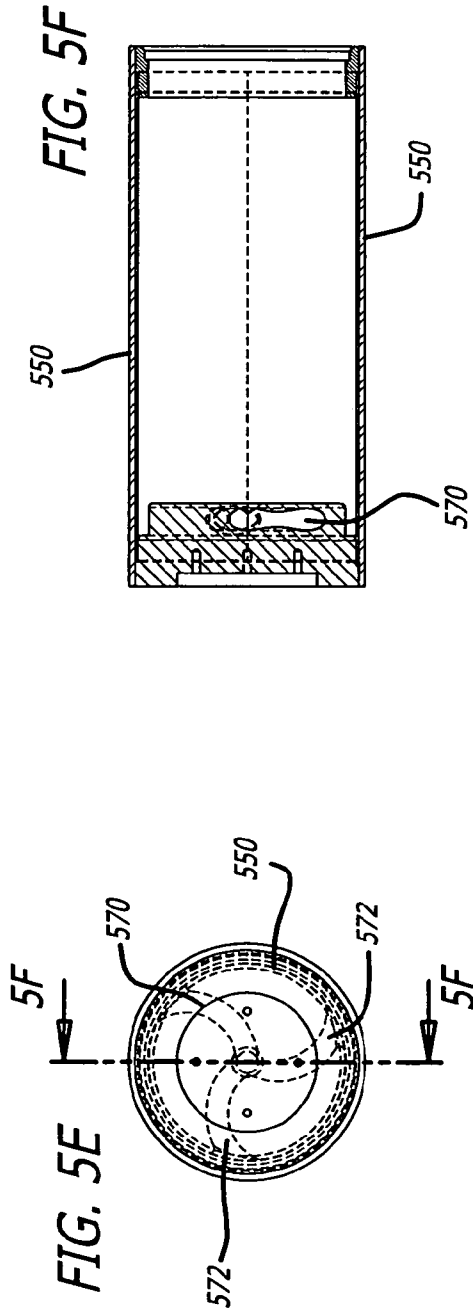


FIG. 5D



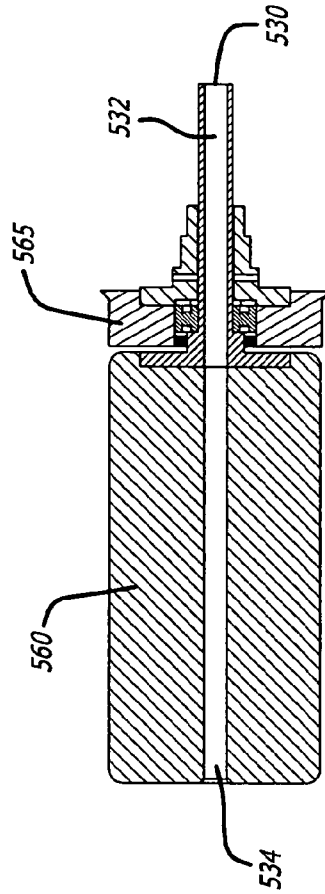
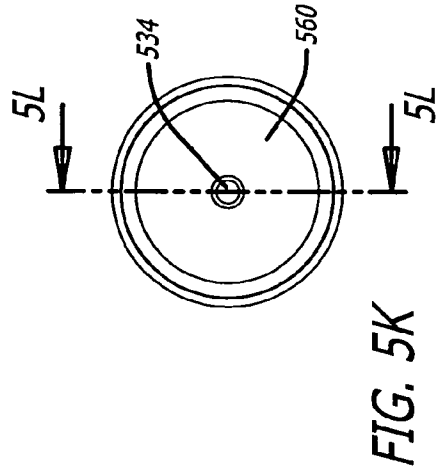
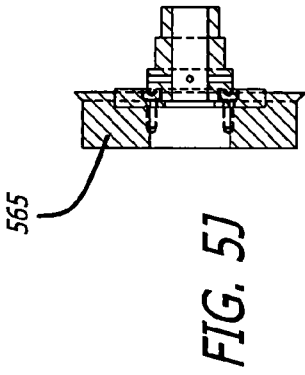
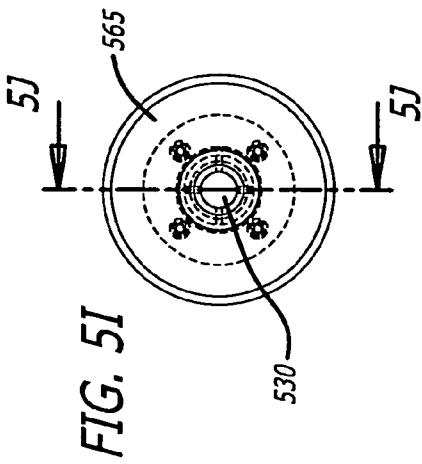
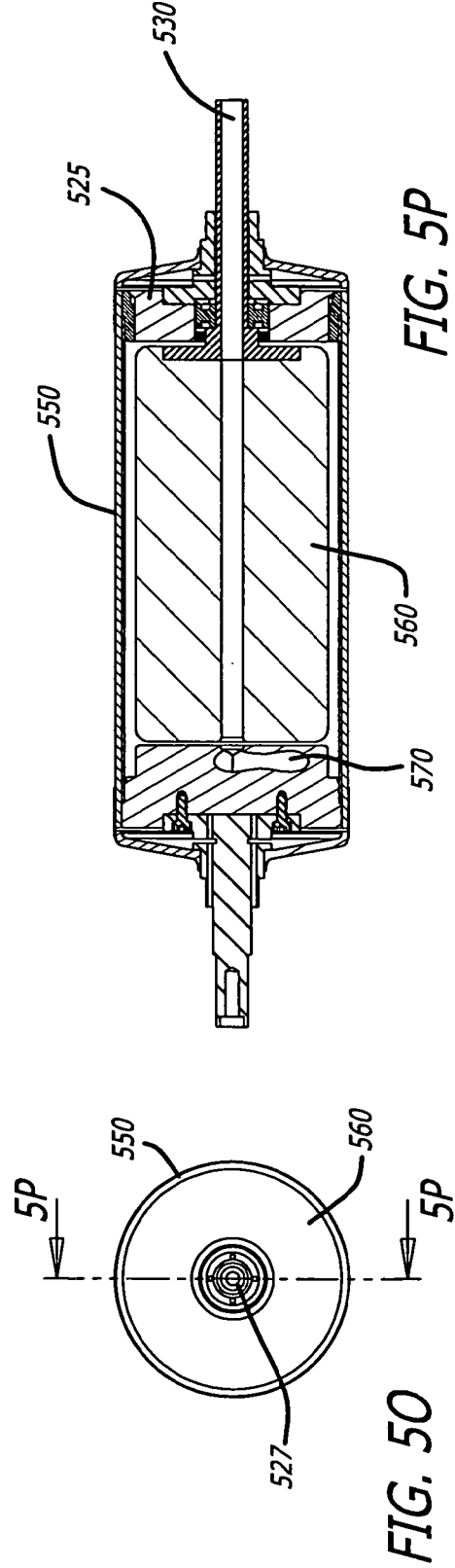
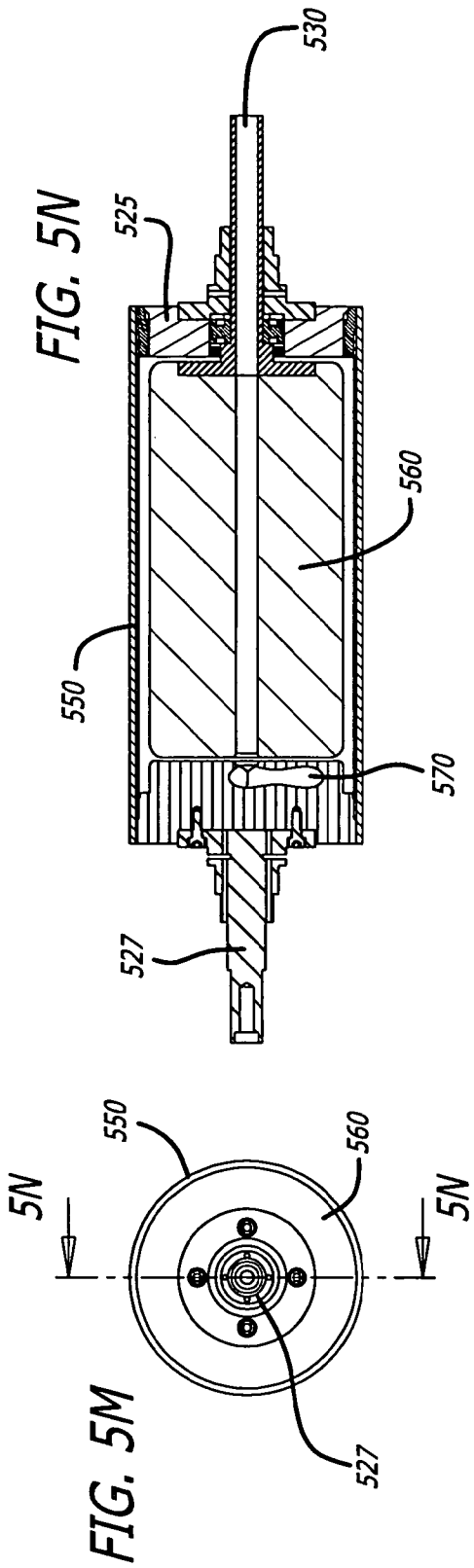


FIG. 5L



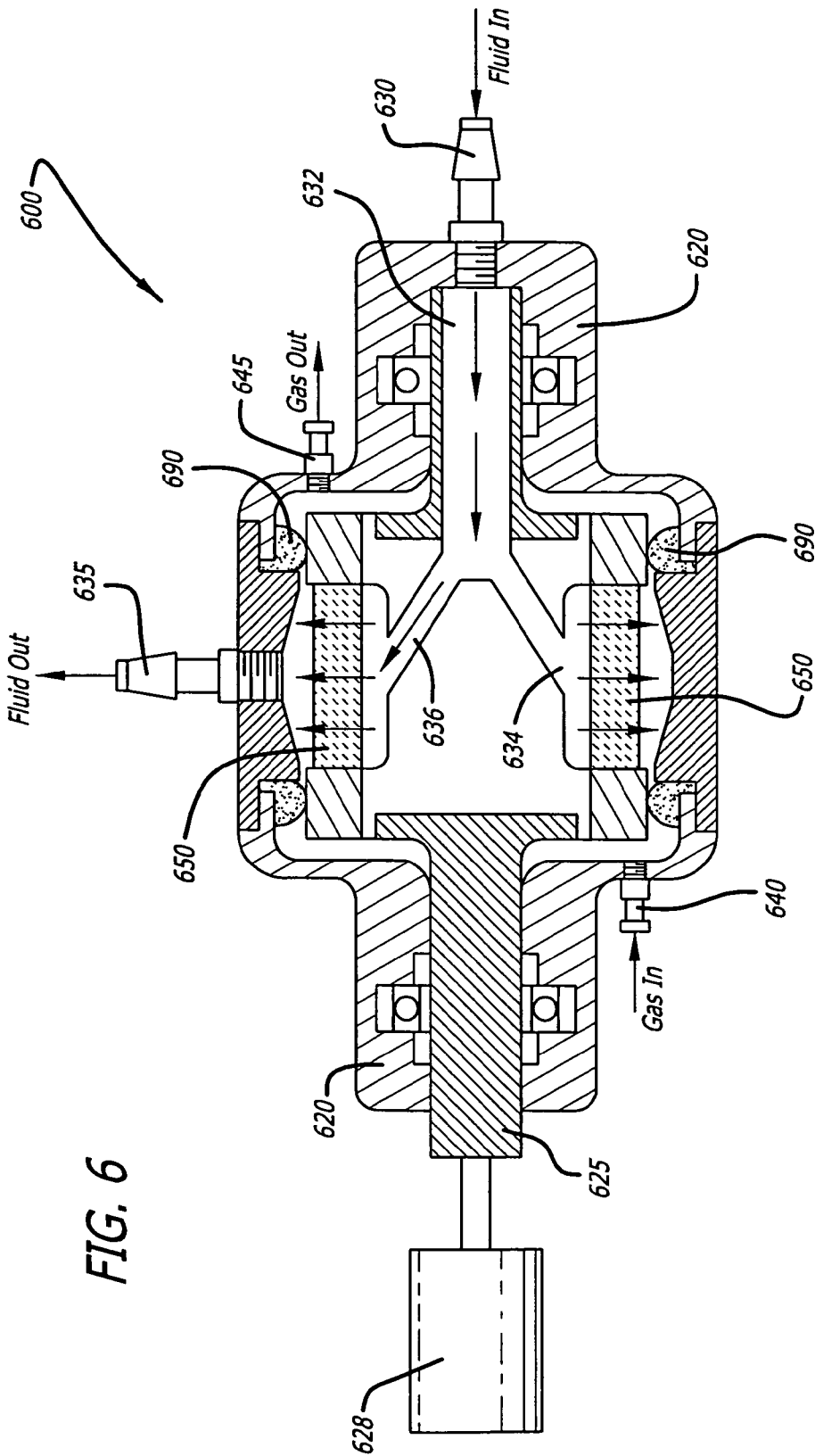


FIG. 6

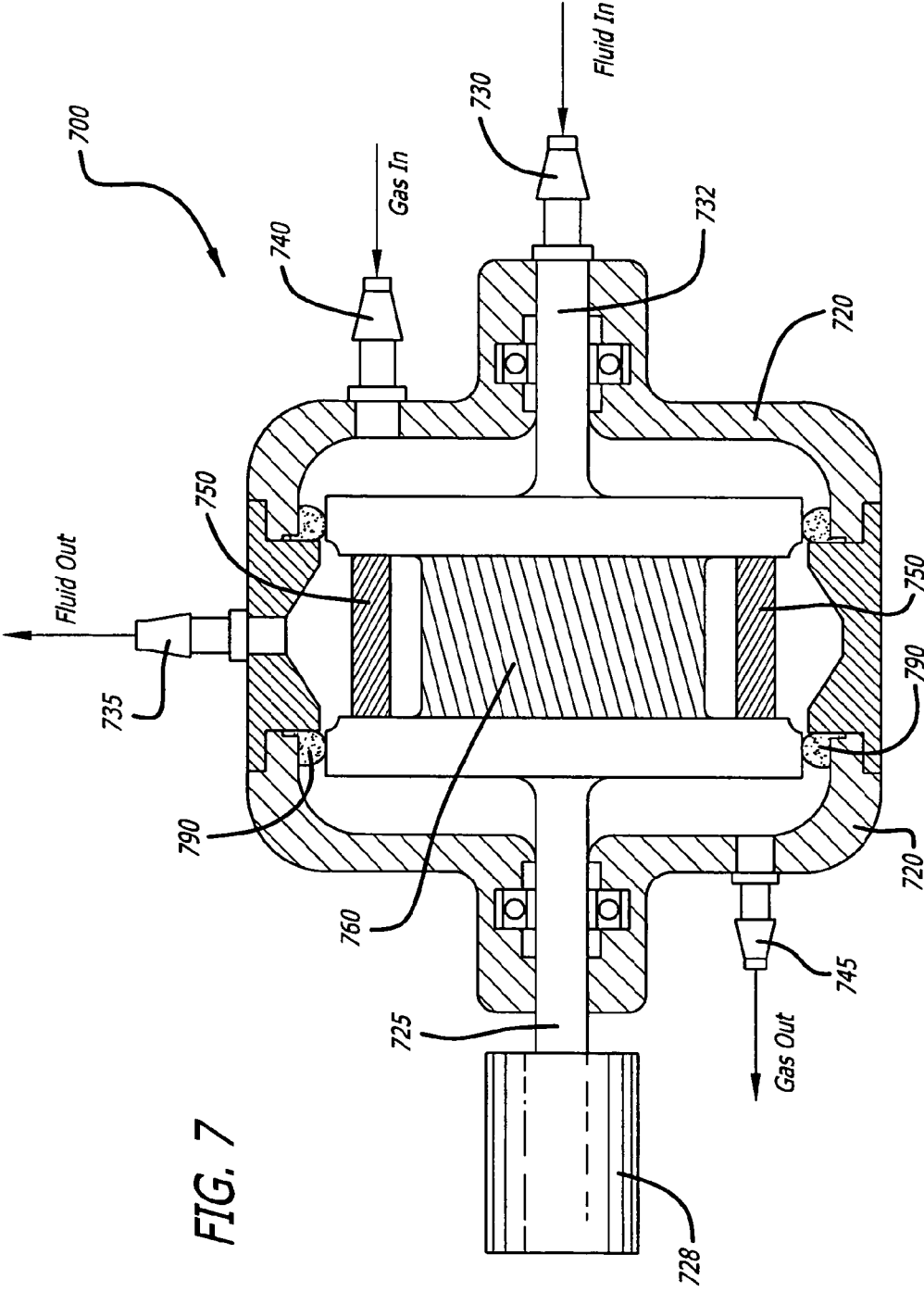


FIG. 7

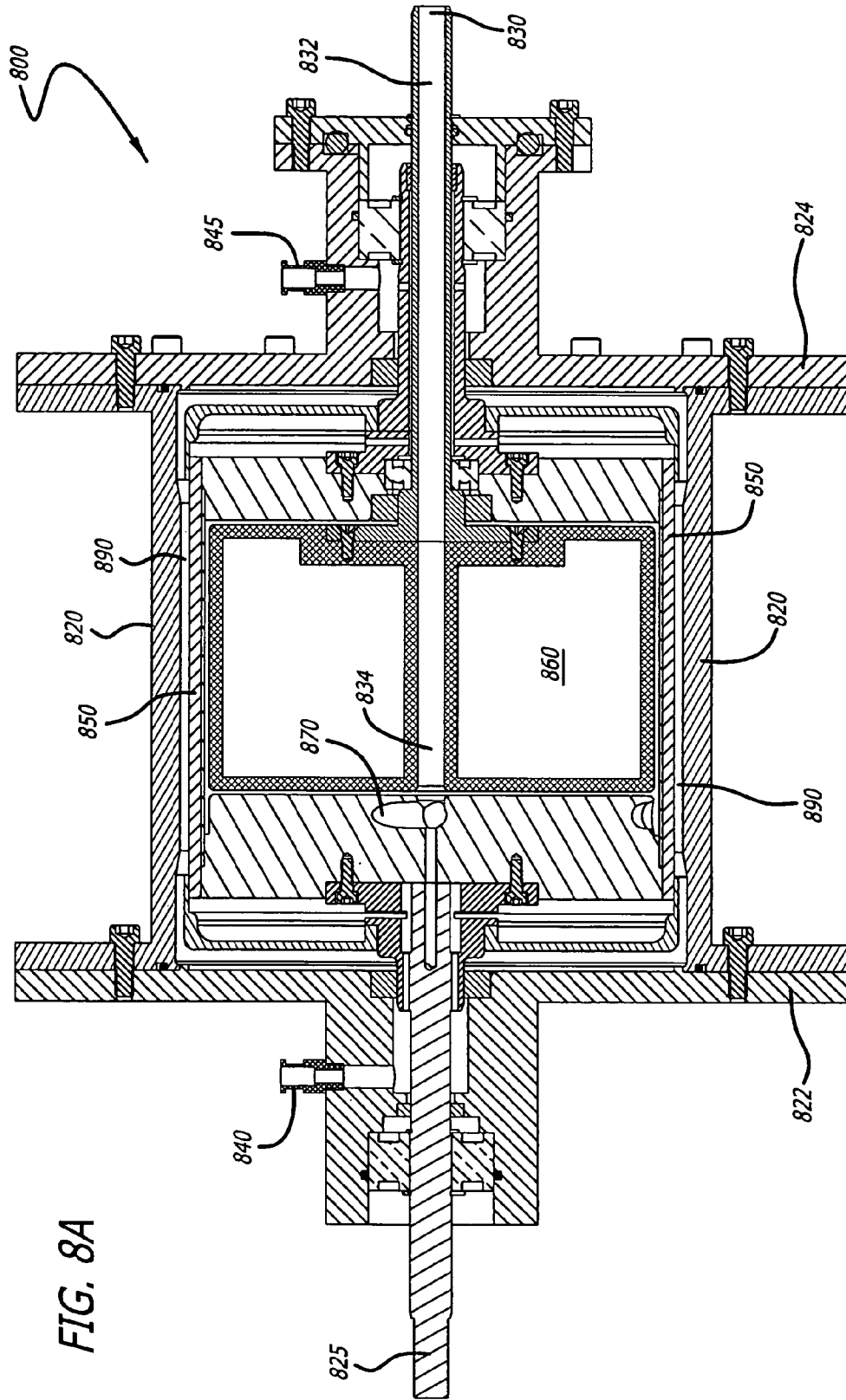


FIG. 8A

FIG. 8B

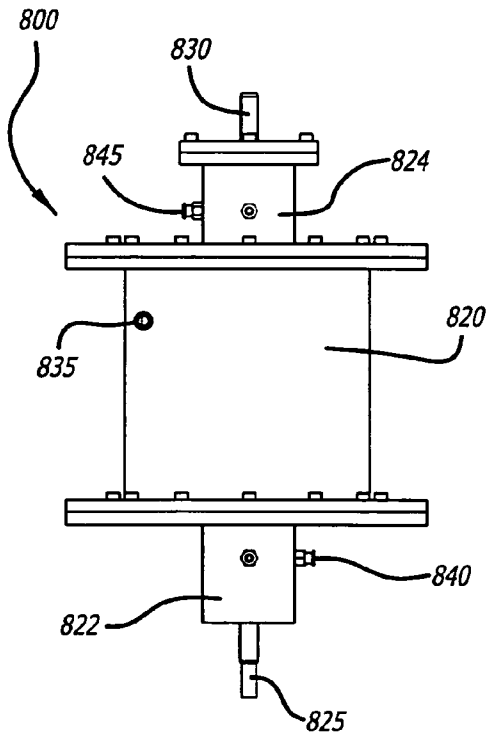
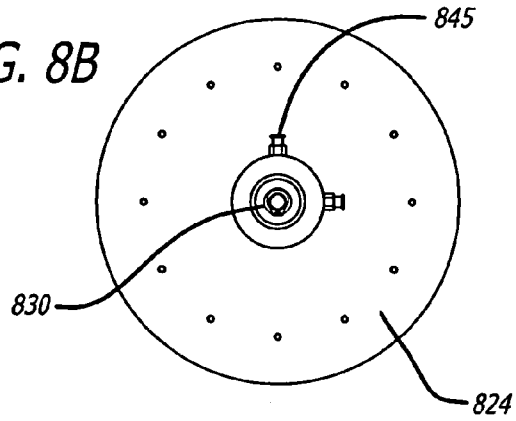


FIG. 8C

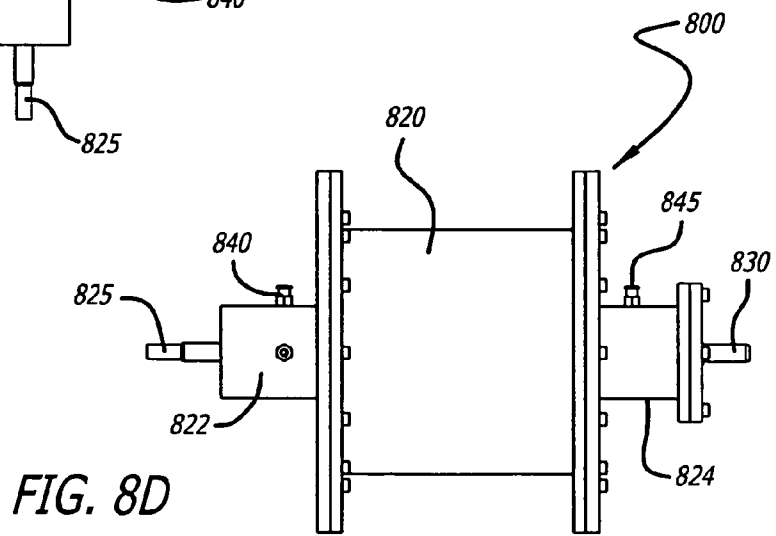


FIG. 8D

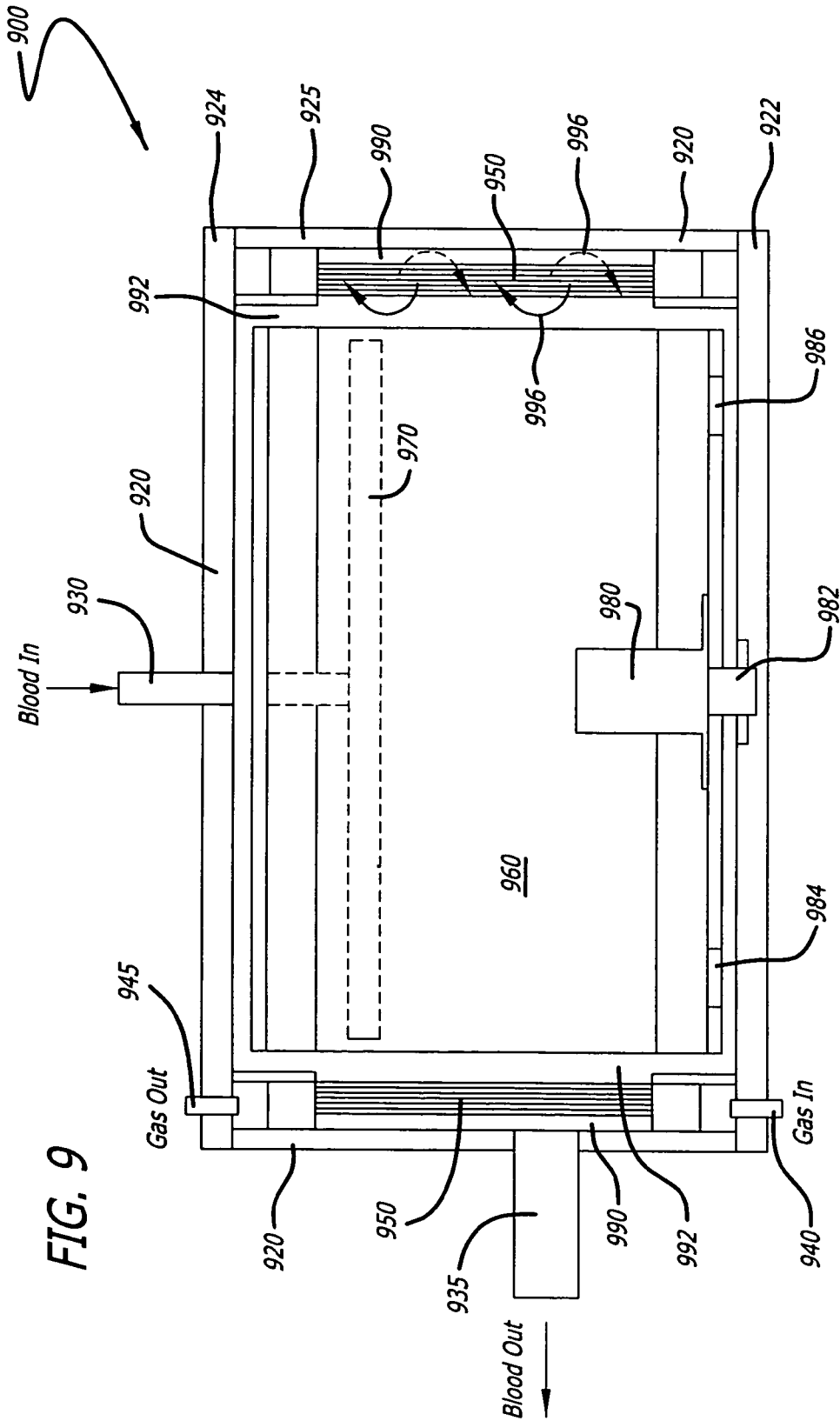


FIG. 9

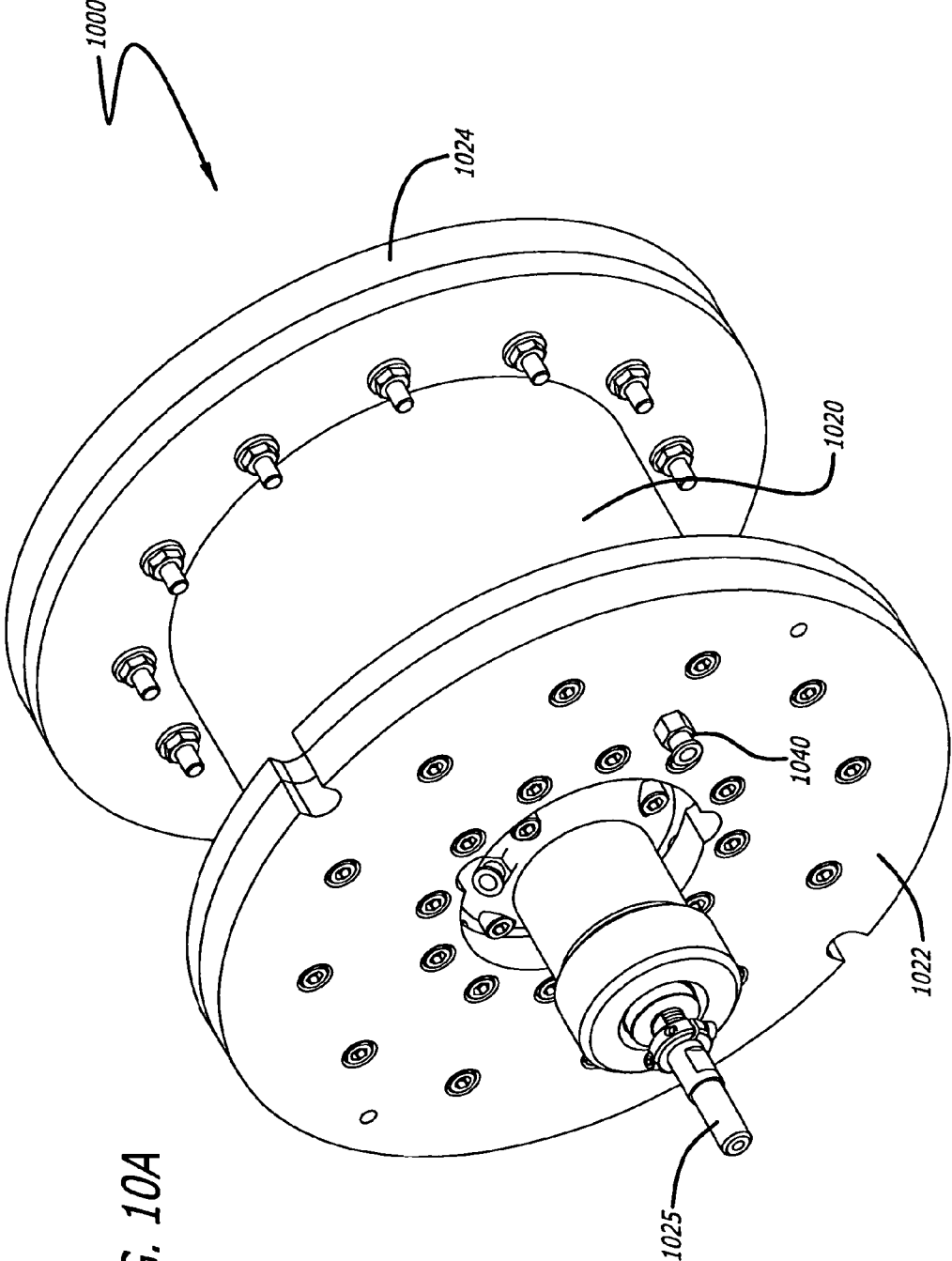


FIG. 10A

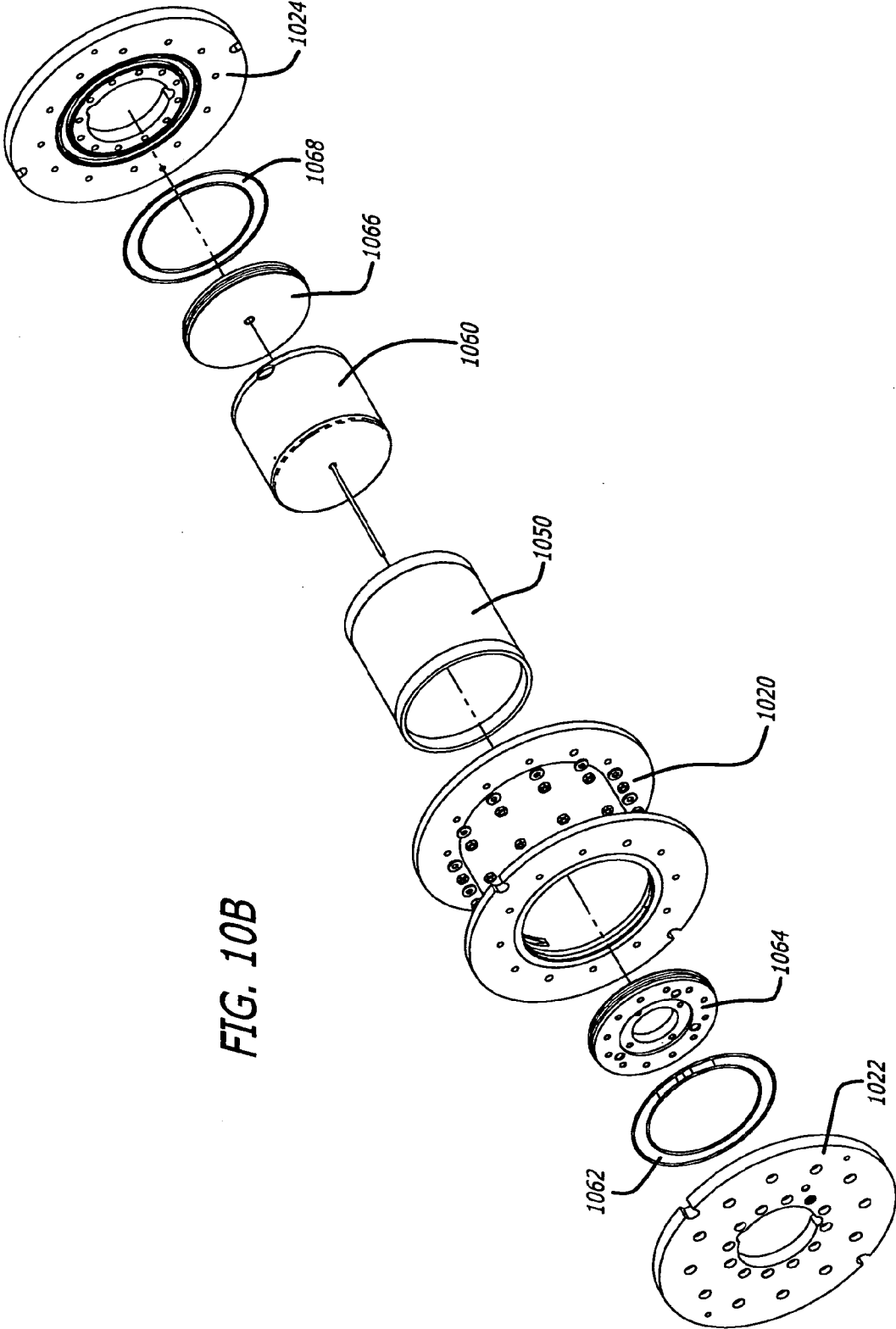


FIG. 10B

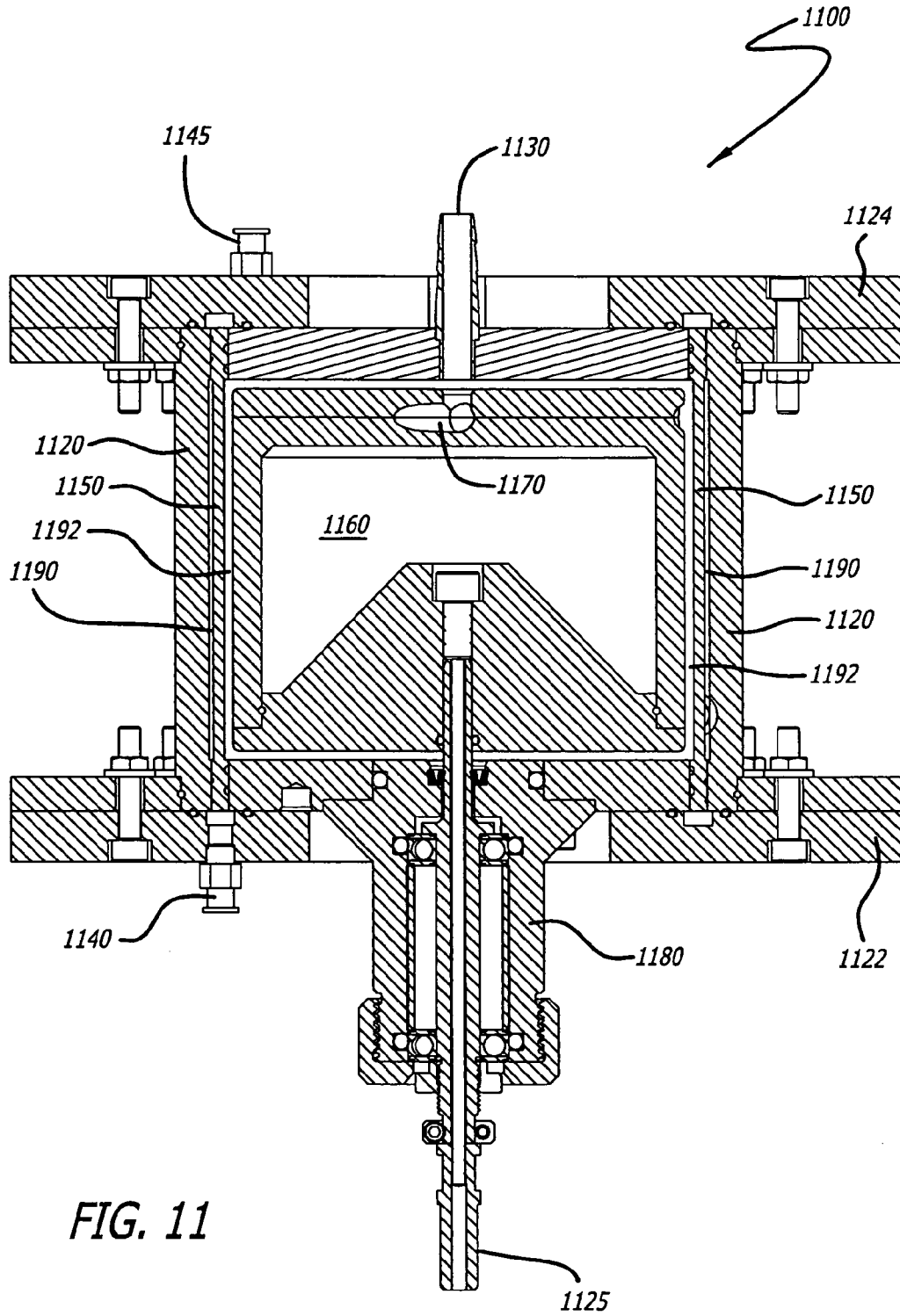


FIG. 11

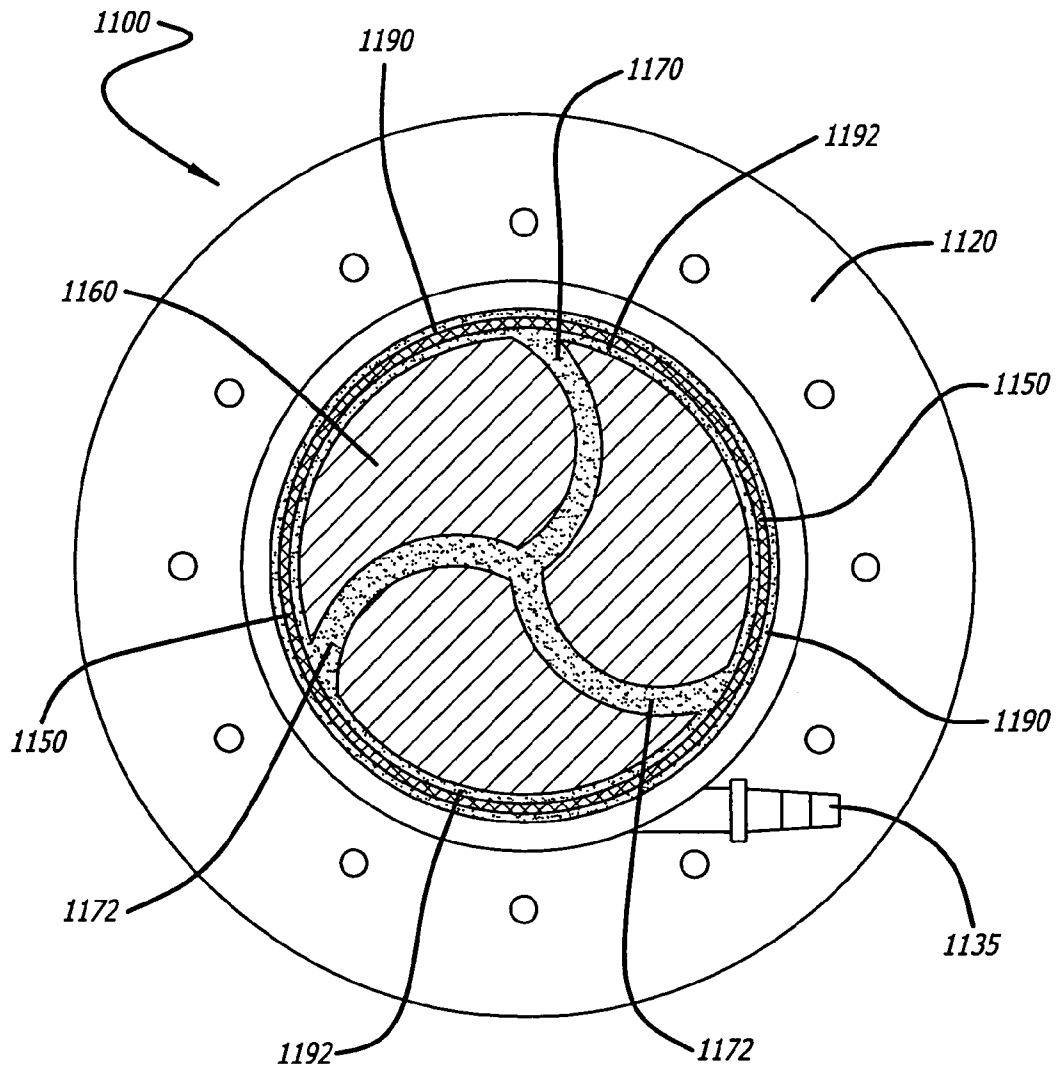


FIG. 12A

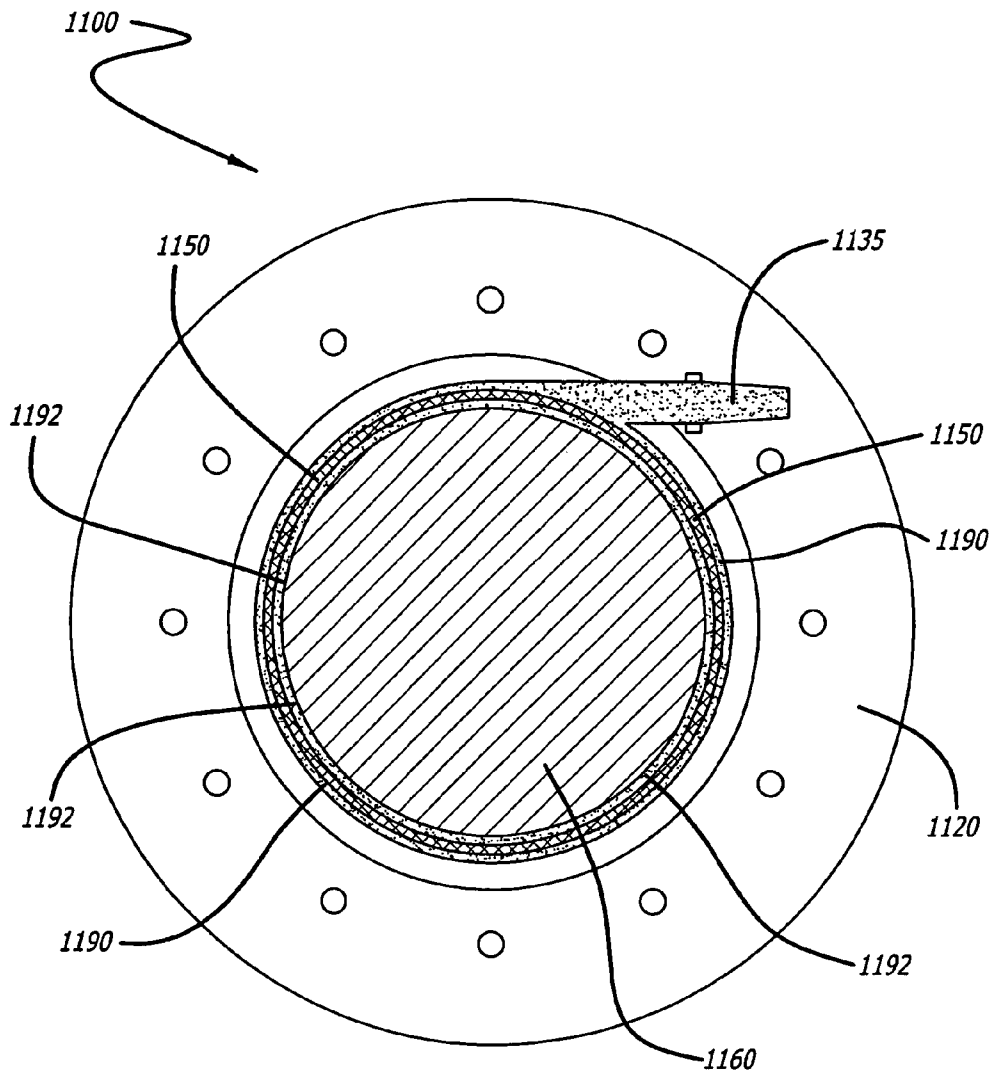


FIG. 12B

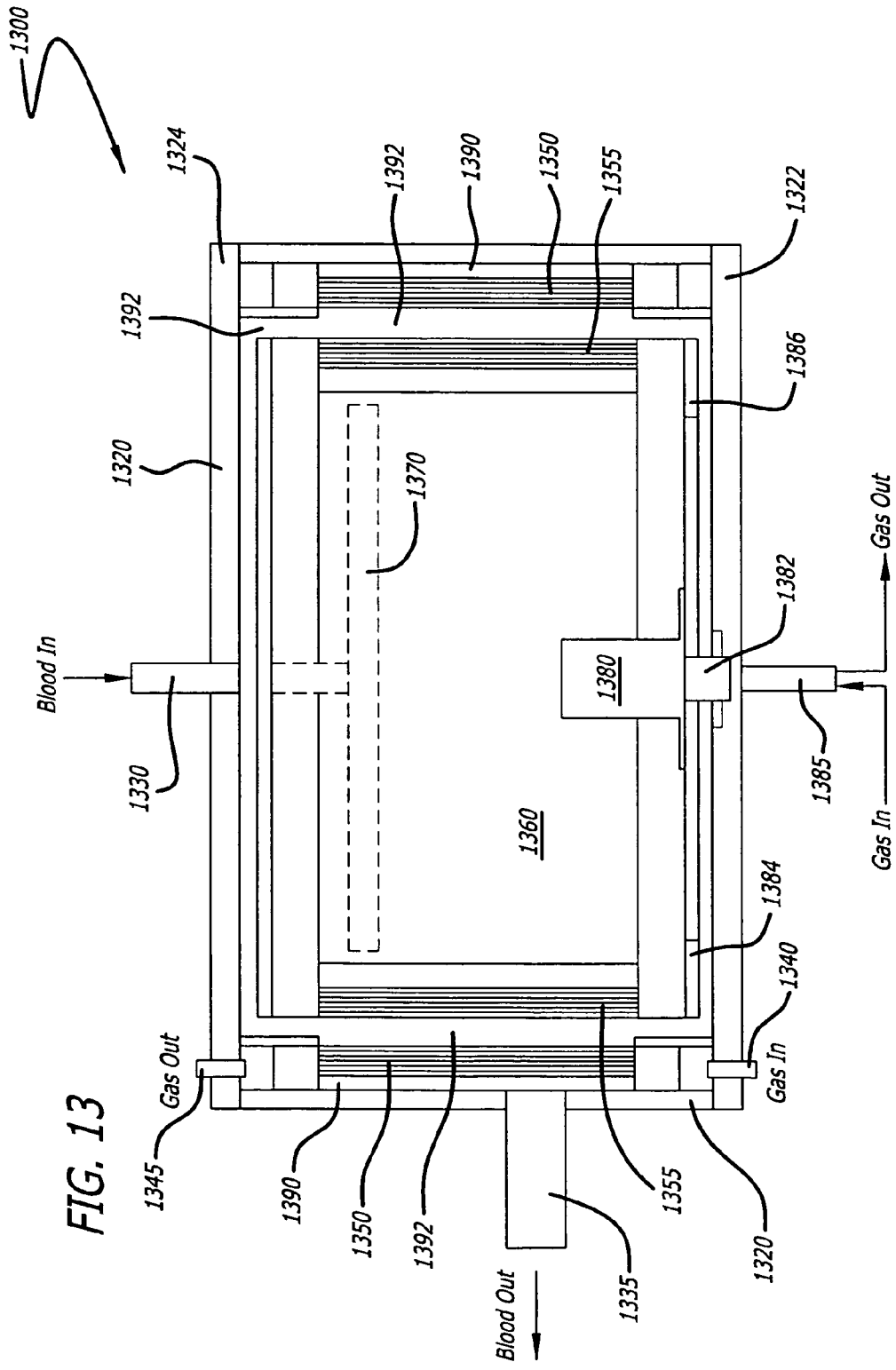


FIG. 13

FIG. 14

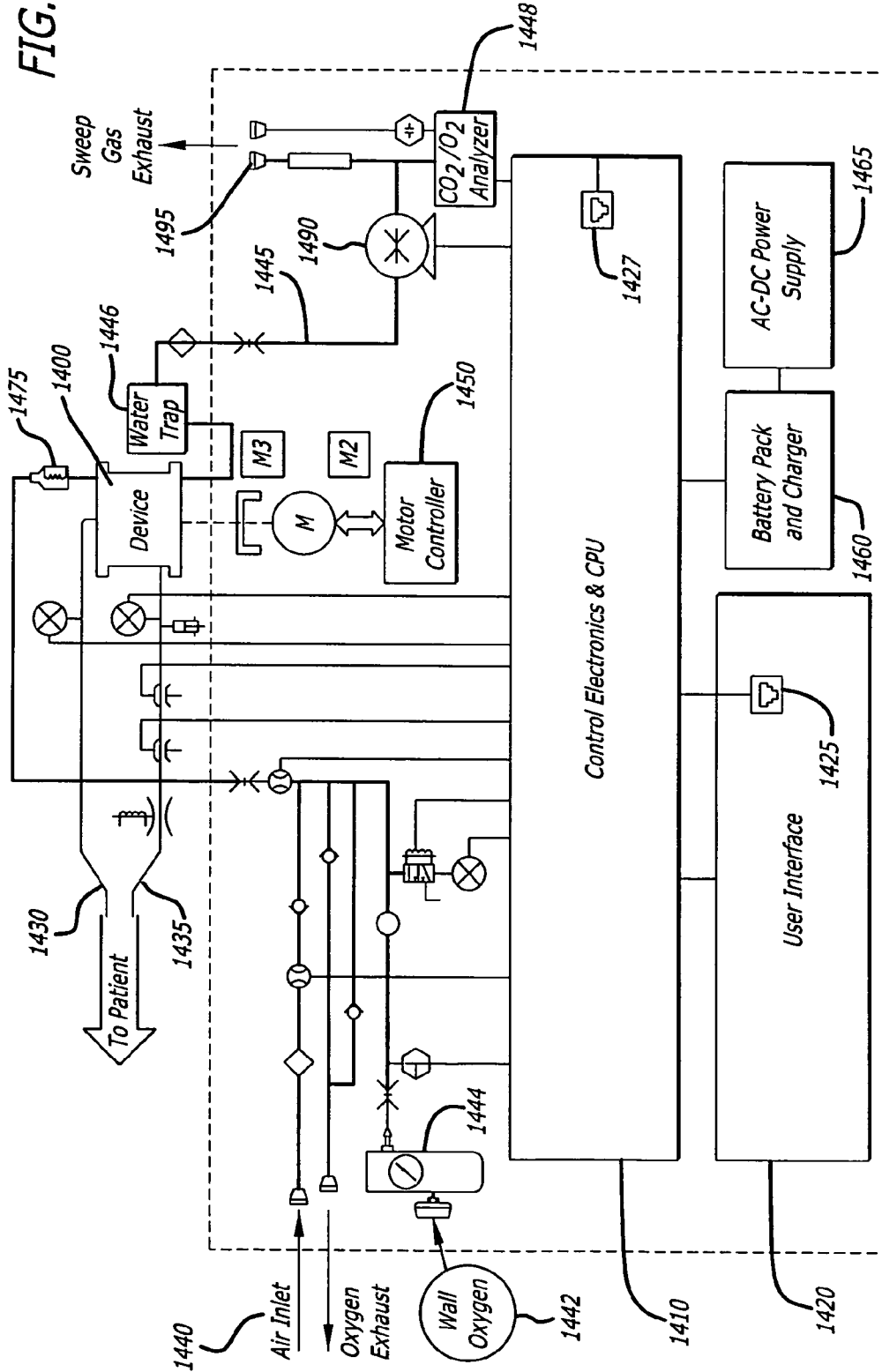
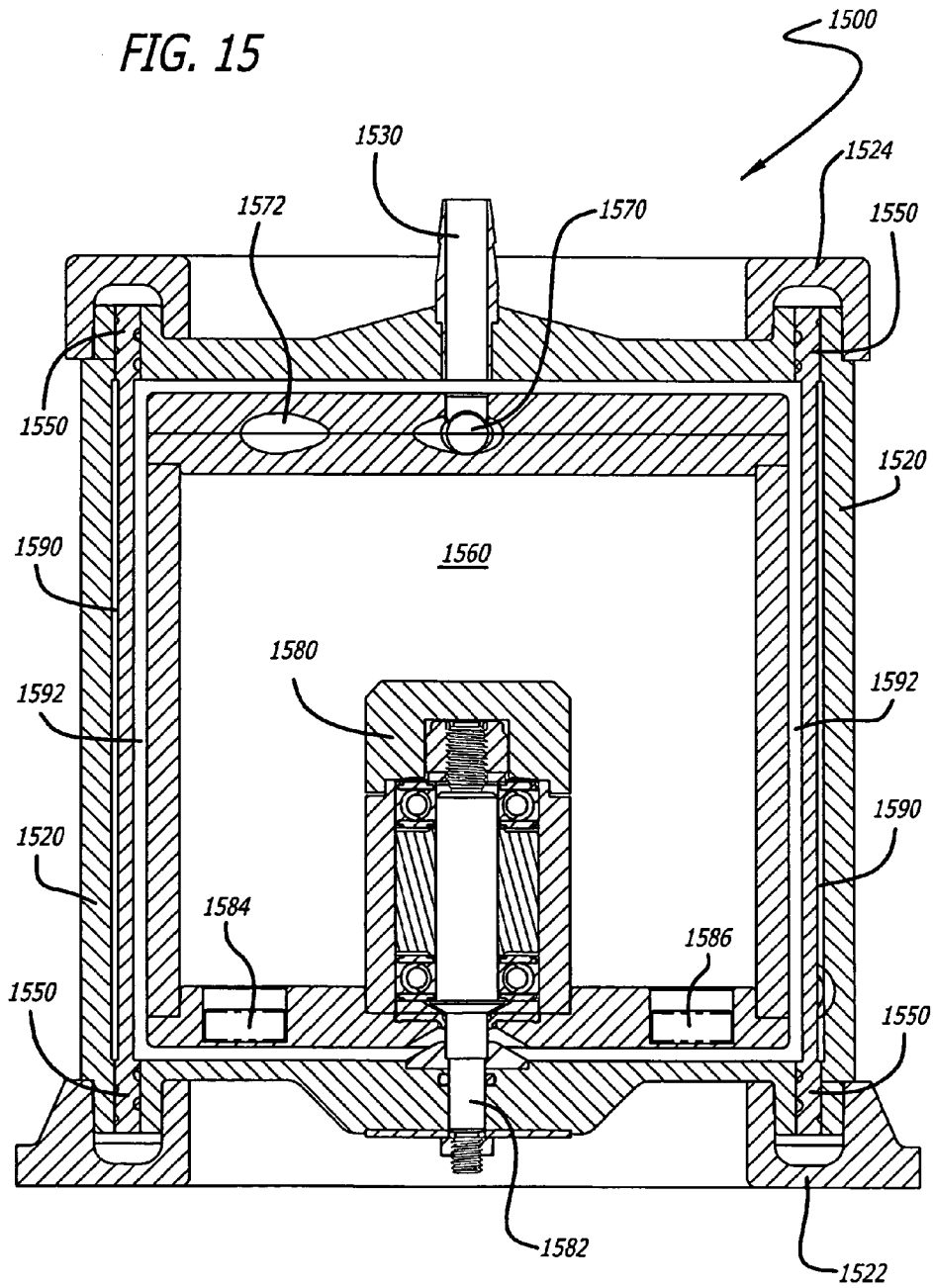


FIG. 15



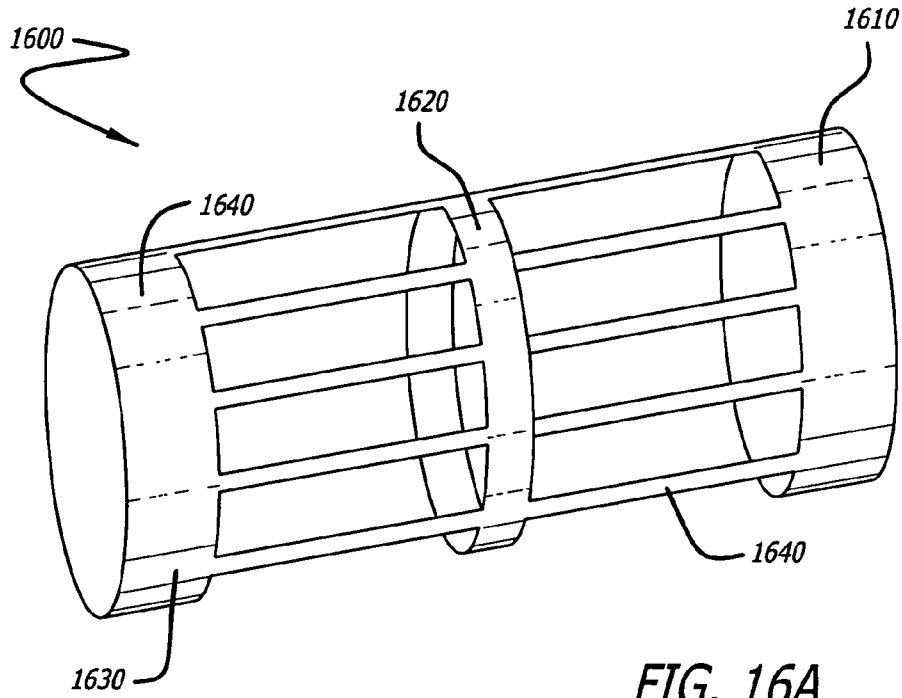


FIG. 16A

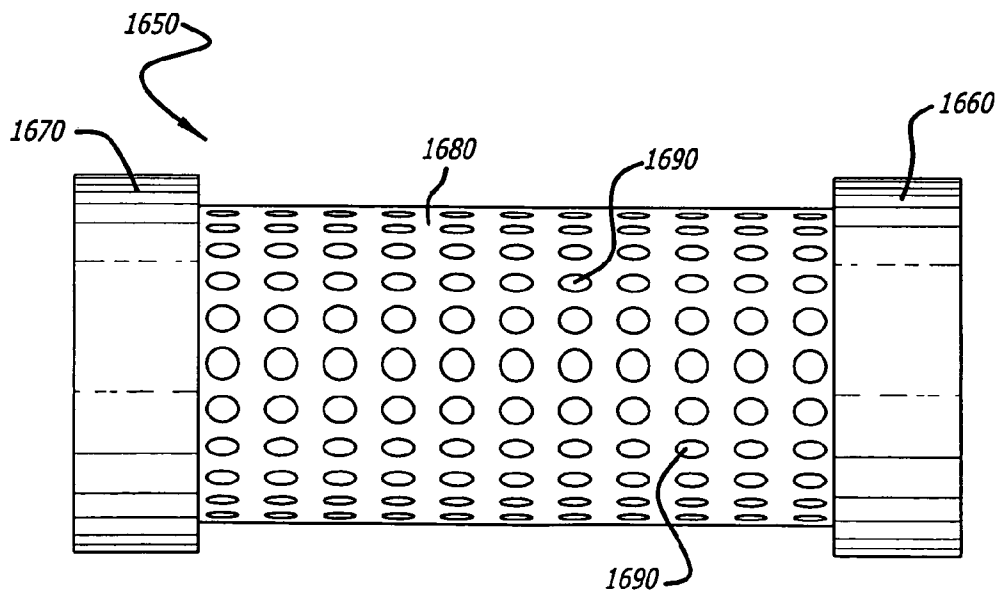


FIG. 16B

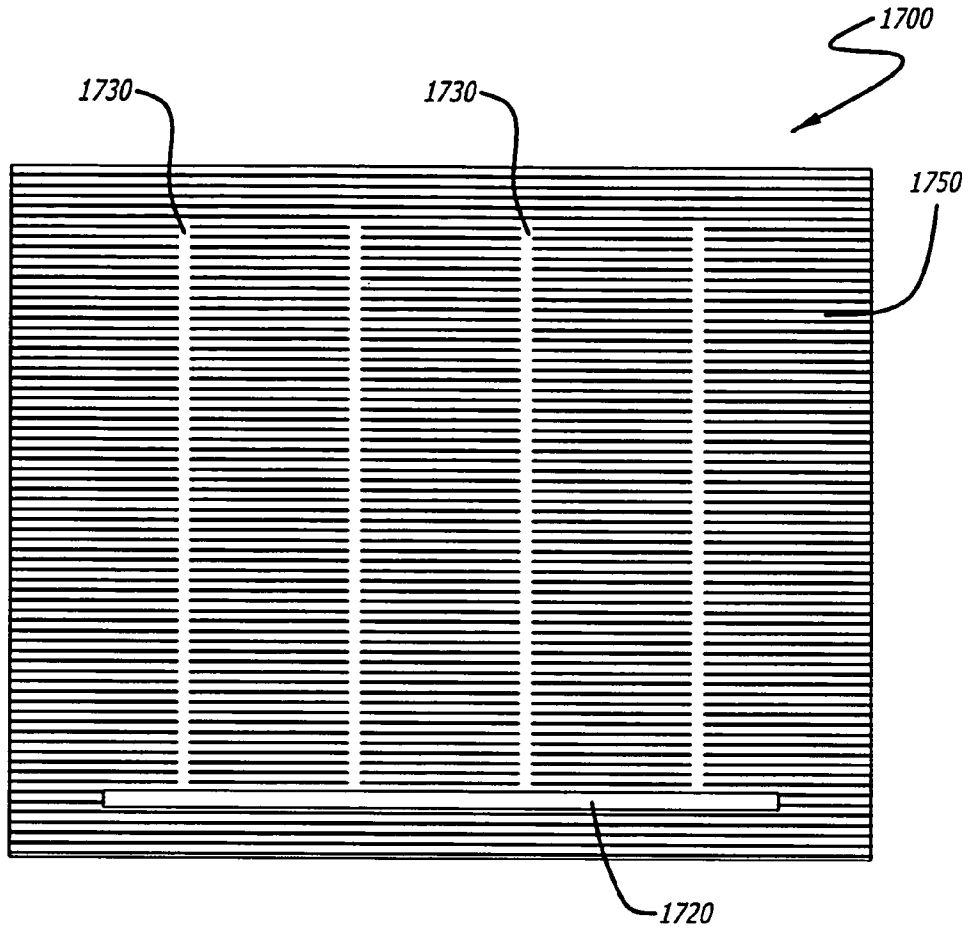


FIG. 17A

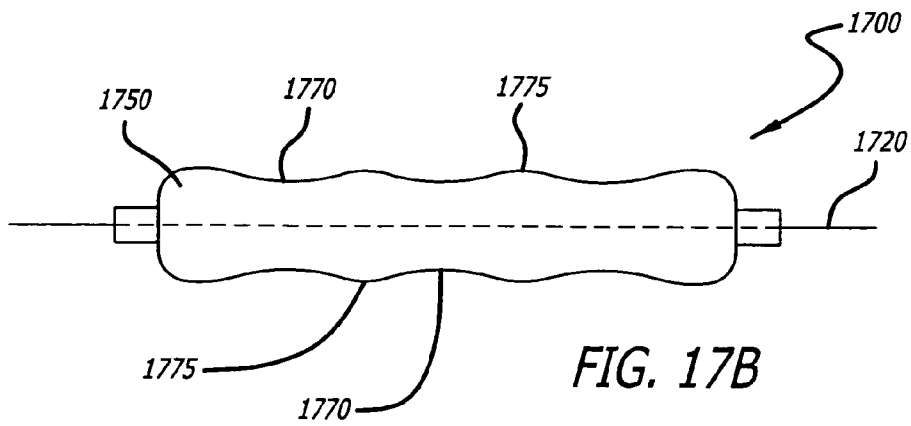


FIG. 17B

FIG. 18

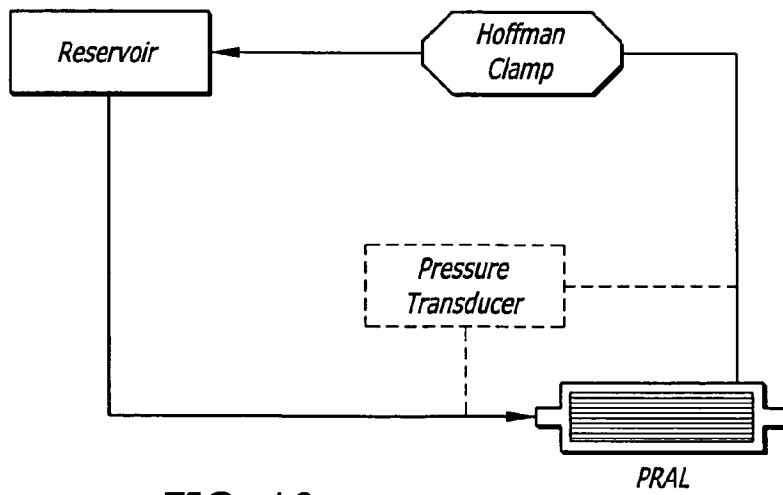
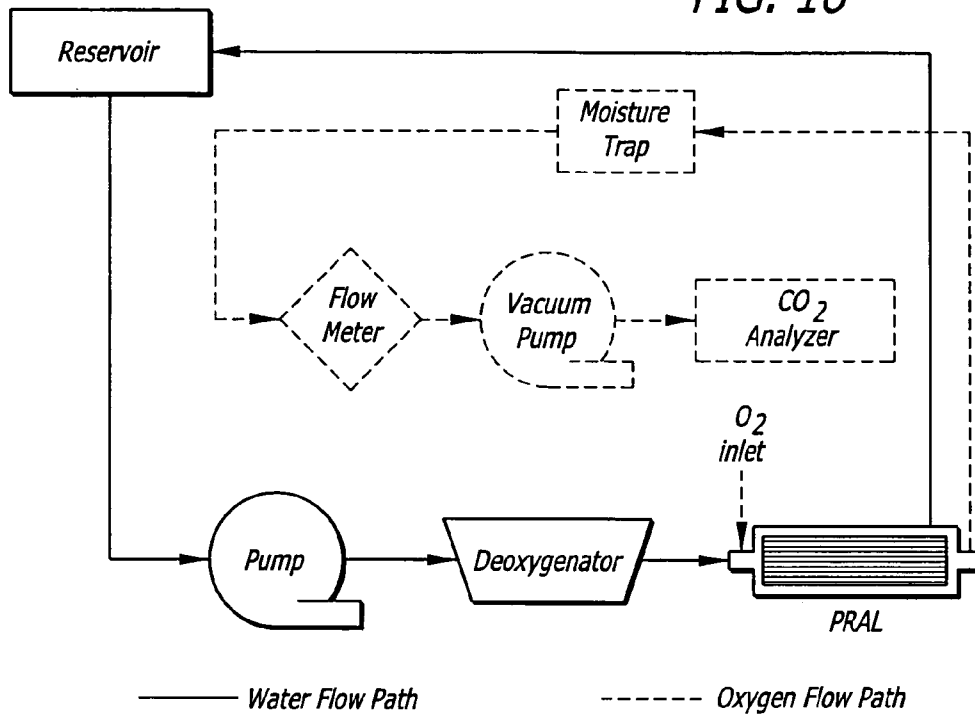


FIG. 19

FIG. 21

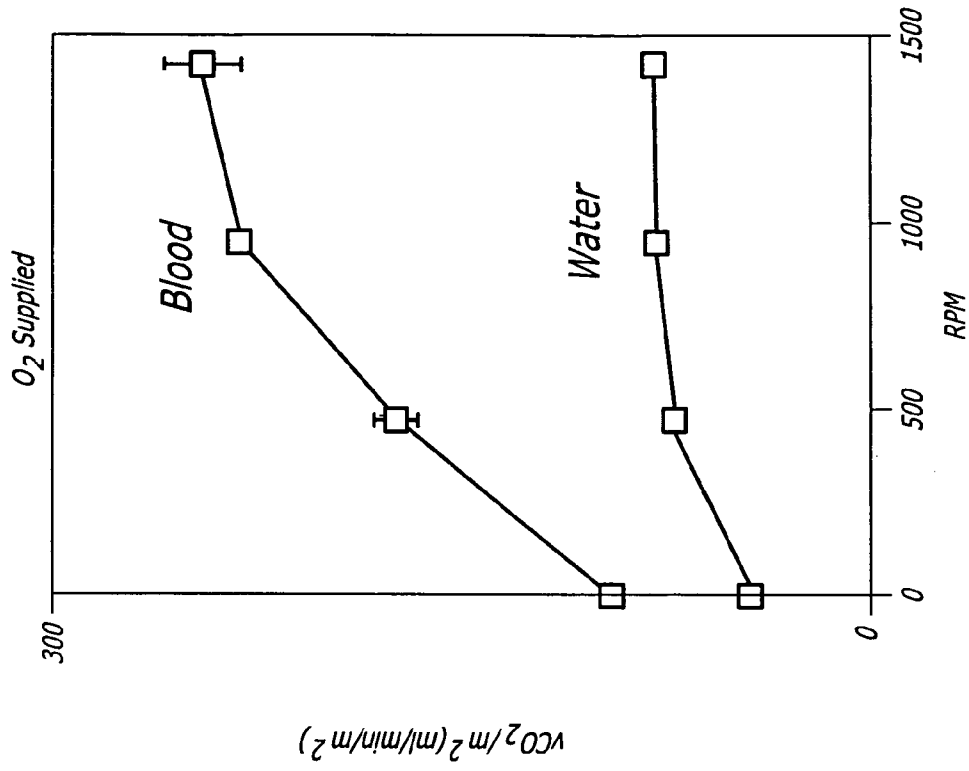


FIG. 20

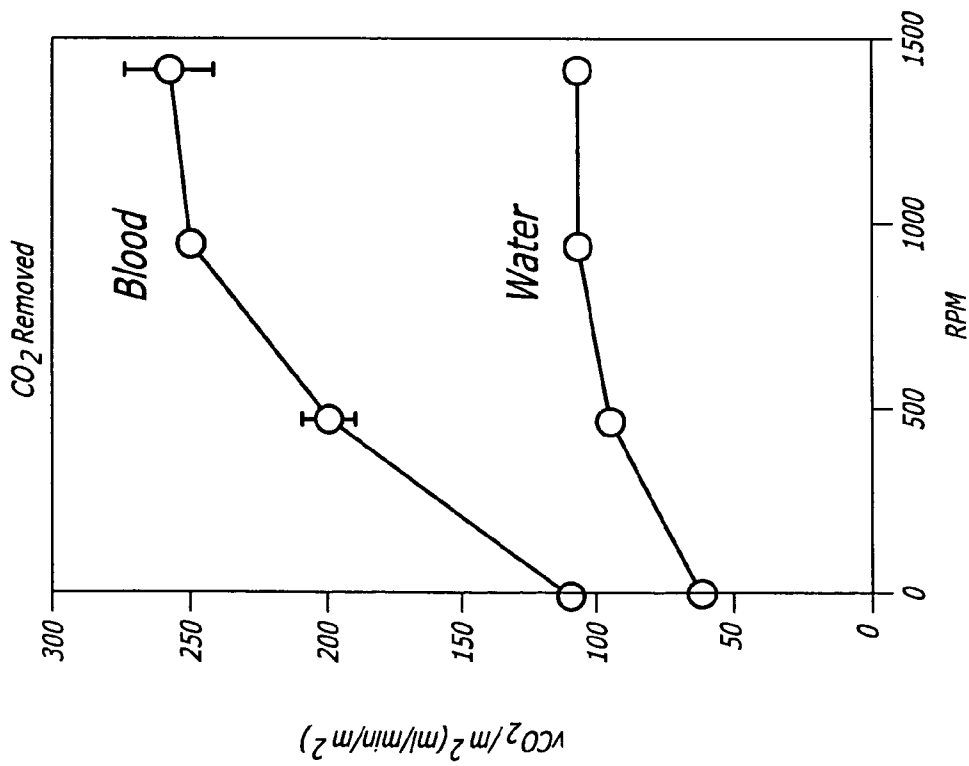
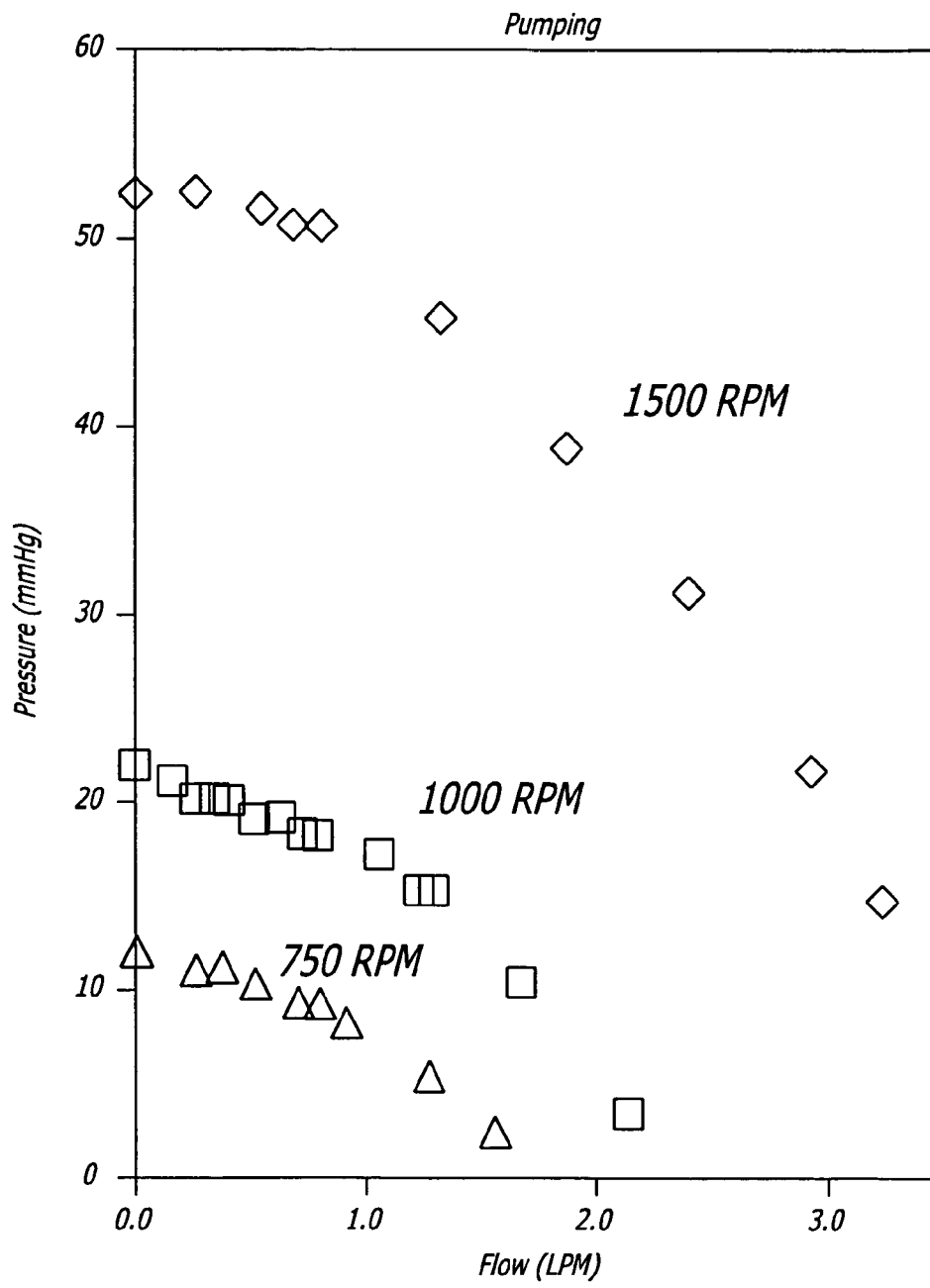


FIG. 22



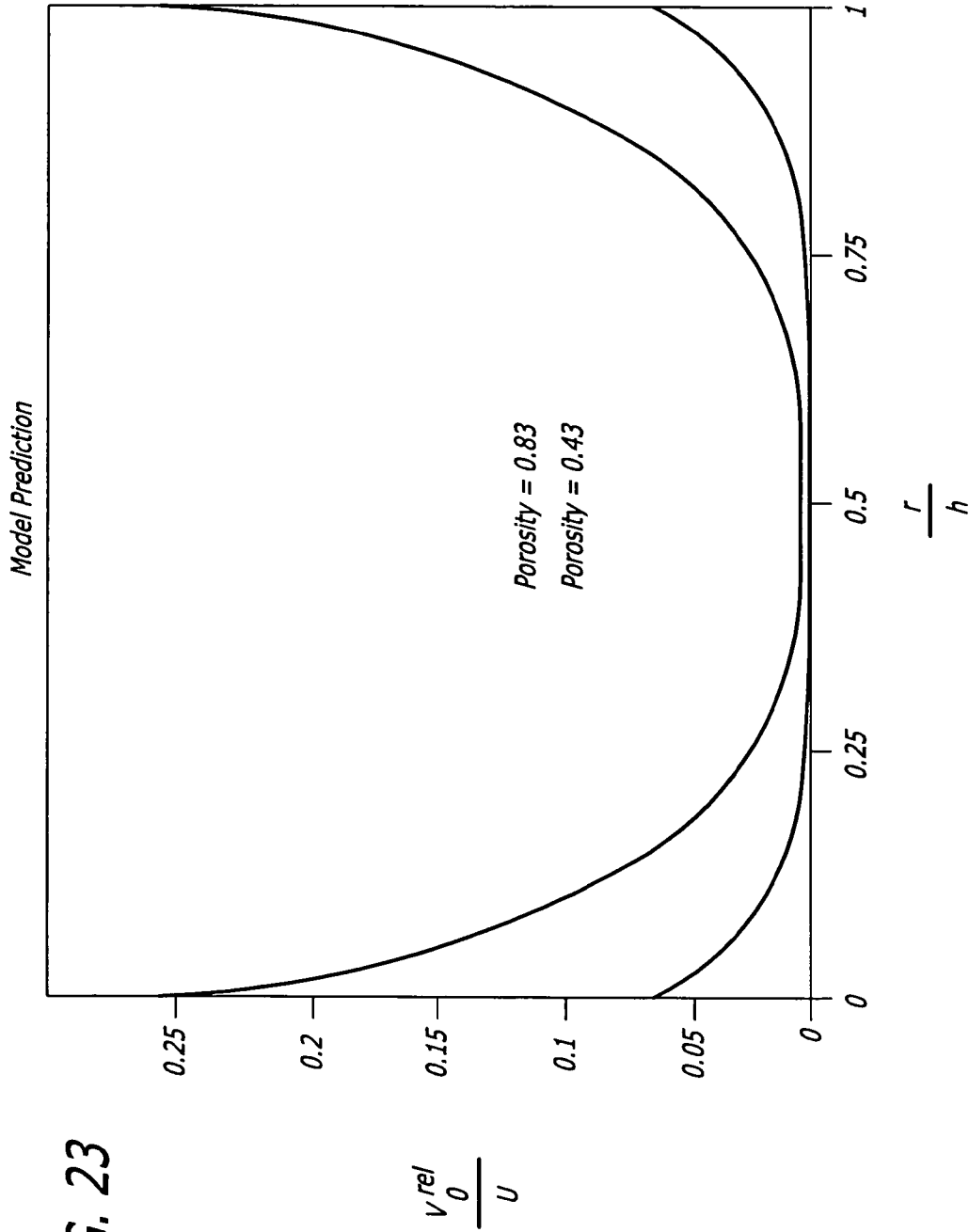


FIG. 23

FIG. 25

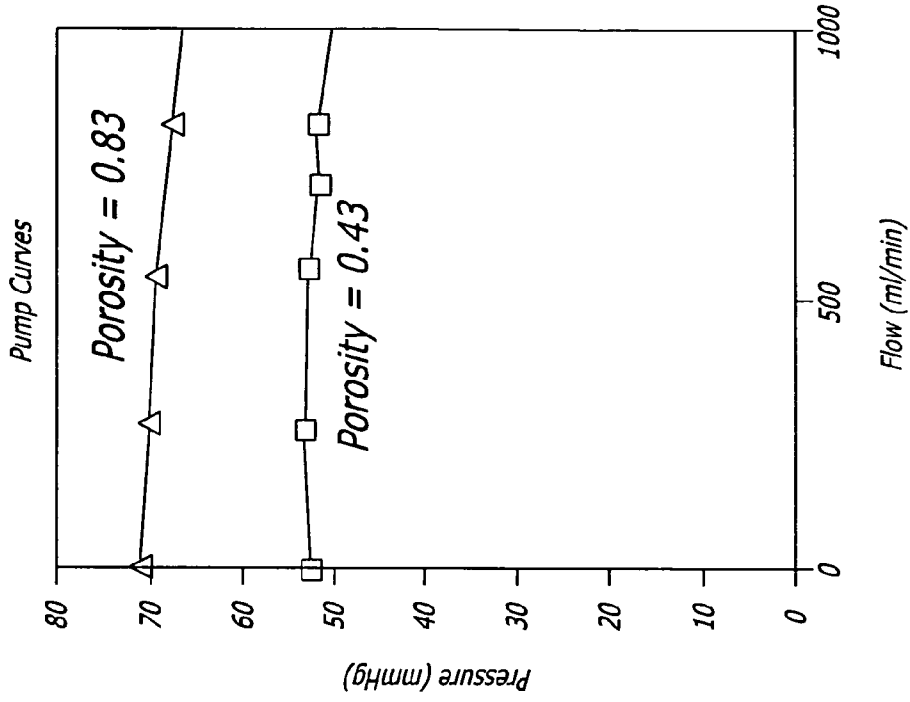
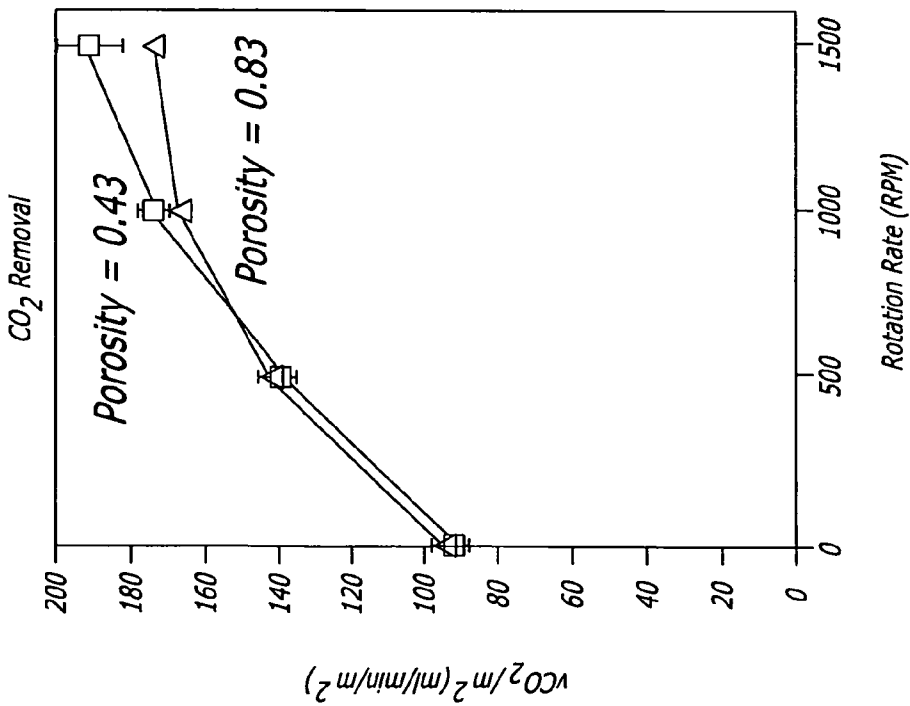


FIG. 24



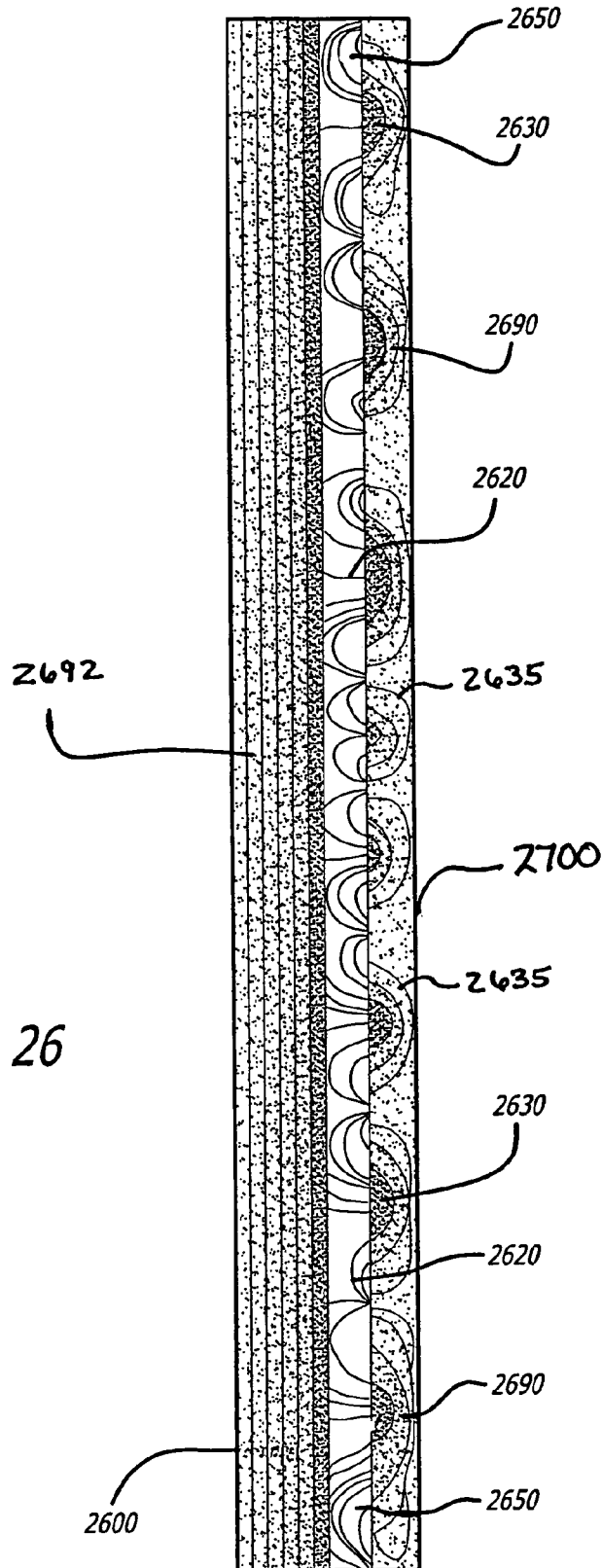


FIG. 26

PARACORPOREAL RESPIRATORY ASSIST LUNG

CROSS-REFERENCES TO RELATED APPLICATIONS

This is a divisional application which is based on U.S. Ser. No. 11/408,650, filed on Apr. 21, 2006, U.S. Pat. No. 7,927,544 with an issue date of Apr. 19, 2011; which claims priority from U.S. Provisional Patent Application Ser. No. 60/673,885, filed Apr. 21, 2005 and U.S. Provisional Patent Application Ser. No. 60/688,809, filed Jun. 8, 2005, each of which are incorporated by reference in their entirety.

FEDERALLY SPONSORED RESEARCH

The U.S. Government has a paid-up license in this invention and the right in limited circumstances to require the patent owner to license others on reasonable terms as provided for by the terms of Grant Nos. DAMD 17-02-1-0717 awarded by the Department of the Army and Grant No. RO1 HL 70051 awarded by the National Institutes of Health.

BACKGROUND OF THE INVENTION

The present invention is directed to an improved veno-venous extracorporeal oxygenator, referred to herein as a "paracorporeal respiratory assist lung" or the "PRAL device." More specifically, the paracorporeal respiratory assist lung includes a variable speed (oscillating) rotating fiber bundle having increased porosity. In addition, the PRAL device may be configured to rotate a core wherein the fiber bundle is stationary, and may further be configured to include a fiber bundle on the rotating core.

It has been reported that 350,000 Americans die of lung disease each year, most from Acute Respiratory Distress Syndrome (ARDS) and Chronic Obstructive Pulmonary Disease (COPD). The most common treatment is mechanical ventilation, but may further exacerbate respiratory insufficiency and can cause serious side effects, such as barotrauma and volutrauma. It has been further reported that heart-lung machines, which utilize oxygenators, are employed during surgery throughout the world hundreds of thousands of times per year. Such oxygenators may be useful in treating COPD and ARDS. However, inefficient mass transfer (gas exchange) of oxygen and carbon dioxide is a common problem in oxygenators used in heart-lung machines.

The use of membrane oxygenators to oxygenate blood is well known in the art. One type of conventional membrane oxygenator employs bundles of hollow fibers retained within a cylindrical housing wherein oxygen is pumped through the hollow fibers in the same direction as the blood. The hollow fibers consist of a microporous membrane which is impermeable to blood and permeable to gas. Gas exchange takes place when venous blood flows through the housing and contacts the hollow fibers. Based on the law of diffusion, the oxygen diffuses across the hollow fiber walls and enriches venous blood in contact with these hollow fibers. A stated disadvantage to this type of membrane oxygenator is that a blood boundary layer is formed around the hollow fibers which retards oxygenation of blood that does not directly contact the hollow fibers.

Another known type of membrane oxygenator includes moving a portion of the oxygenator to provide increased mixing of blood flow. In this type of membrane oxygenator, a blood flow path and an oxygen flow path are positioned between a rotor and a stator and separated by a membrane and

a wafer. When the rotor rotates relative to the stator, mixing of blood flow occurs resulting in disruption of the blood boundary layer. Although such an oxygenator provides a degree of mixing of blood, this mixing may cause destruction of red blood cells. In one embodiment of such an oxygenator, a cylindrical, semi-permeable membrane containing oxygen is rotated in a housing such that blood contacts and flows over the membrane and oxygen is transferred through the rotating membrane to the blood. One reported problem with this type of membrane oxygenator is the poor permeability to oxygen and carbon dioxide of semi-permeable membranes.

Yet another known membrane oxygenator includes hollow fiber membranes that extend substantially longitudinally, first inert fibers are spaced between them and also extend substantially longitudinally. Second inert fibers extend generally transverse to the hollow fibers and generally contiguous therewith, so that an oxygen-containing gas can pass through the hollow fibers and blood can be passed over their exterior for gas exchange through the membrane. The second inert fibers may form a weft and the first inert fibers are spaced one between each two hollow fibers so that the warp consists of alternating strands of hollow fiber and first inert fiber passing over the weft in an oscillating fashion. The inert fibers are disclosed as biocompatible monofilament polymers that provide spacing of the hollow fibers to produce even blood films. However, such an oxygenator is not designed for extracorporeal applications having relatively low blood flow rates.

Accordingly, there is a need for, and what was heretofore unavailable, an extracorporeal oxygenator having enhanced gas exchange characteristics resulting from a variable rotating fiber bundle and/or increased porosity of the fiber bundle that has high gas exchange efficiency with minimal damage to the blood components.

SUMMARY OF THE INVENTION

The present invention is directed to an improved veno-venous extracorporeal oxygenator, referred to herein as a "paracorporeal respiratory assist lung." The veno-venous artificial lung may be used as replacement therapy for mechanical ventilation for chronic obstructive pulmonary disease (COPD) patients with high levels of partial pressure of carbon dioxide ($p\text{CO}_2$) in their blood. The paracorporeal respiratory assist lung of the present invention provides active mixing through rotation of a module containing gas-permeable, hollow fibers (annular fiber bundle) for enhanced gas exchange at constant flow rates of blood through the device. Rotation of the fiber bundle is known to increase the gas exchange efficiency of artificial lungs, for example, a two-hundred percent increase in carbon dioxide (CO_2) transfer efficiency. It has been demonstrated that CO_2 removal of 100-120 milliliters per minute (ml/min) can be achieved with blood flow rates in the range of 0.5 to 1.0 liters per minute (l/min). The rotating fiber bundle provides self-pumping of blood through the device with pressure heads below thirty millimeters of mercury (mmHg). It has been demonstrated that self-pumping of blood through the device with pressure heads that can be tailored to the application by altering the diameter of the annular fiber bundle or the speed of rotation. Prototypes with fiber bundle diameters up to 4 inches size have generated pressure heads up to 100-300 mmHg. Accordingly, the paracorporeal respiratory assist lung acts as an integrated pump/hollow fiber membrane mass transport device.

One aspect of the improvements to the paracorporeal respiratory assist lung according to the present invention includes an annular cylindrical hollow fiber membrane device

that is rotated at rapidly varying speeds. Fluid is introduced to the center of the device and is passed radially through the fiber bundle. The bundle is rotated at rapidly changing velocities with a rotational actuator (usually a motor). It has been demonstrated that the present invention enhances mass transfer when the rotational velocity of the fiber bundle is rapidly varied. For example, oscillations are introduced in the steady rotation of a hollow fiber bundle to increase the mass transfer efficiency of the device while maintaining its pumping capabilities.

Another aspect of the improvements to the paracorporeal respiratory assist lung according to the present invention includes increasing the porosity in the rotating fiber bundle. The increased porosity provides more fluid to flow through the fiber bundle, thus increasing the overall mass transfer efficiency of the device. The extra porosity in the fiber bundle is created by several possible ways including, but not limited to, using spacers to create void space between the fiber layers, removing every other fiber in the mat and using smaller diameter fibers. Additionally, support threads could be removed from the fiber fabric, and the paracorporeal respiratory assist lung could be configured such that the manifolds are relatively closer so as to "puff out" the fiber bundle.

A further aspect of the present invention includes a paracorporeal respiratory assist lung having the following features:

- Paracorporeal veno-venous system with percutaneous cannula
- Inserted in the venous circulation for blood flow
- Self-pumping of blood flow driven by rotating fiber bundle
- Removes CO₂ and supplies O₂ before blood reaches the lungs
- Gas exchange at blood flow rates of less than one liter per minute
- Rotating hollow fiber bundle for enhanced gas exchange
- Rotating annular fiber bundle promotes increased flow velocity past fiber surfaces
- Stationary core and outer housing generate fluid shear on fiber bundle
- Blood pathway allows rotating bundle to pump fluid
- Compact, efficient hollow fiber module worn externally
- Additional features of the paracorporeal respiratory assist lung of the present invention include:
 - Variable rotation enhances gas exchange
 - Variable porosity of the fiber bundle
 - Blood flows of 500-750 ml/min for respiratory support
 - Small dual-lumen cannula (14-16 French)
 - Active surface area of the fiber bundle is less than 0.50 square meters (m²)
 - CO₂ removal of 100-120 ml/min at blood flow rate of 0.5 to 1.0 liters per minute
 - CO₂ removal independent of the functional capacity of the natural lungs

One embodiment of the present invention includes a paracorporeal respiratory assist lung having a housing having a liquid inlet, a liquid outlet, a gas inlet and a gas outlet. The PRAL device includes a plurality of tubular gas permeable fiber membranes configured to form a fiber bundle, the fiber bundle being disposed within the housing and connected to and in fluid communication with the gas inlet and the gas outlet, wherein a first gap is configured between the housing and the fiber bundle. The device further includes a stationary core being disposed within the fiber bundle, wherein a second gap is configured between the core and the fiber bundle. The PRAL device may be configured for rotating the fiber bundle, wherein the housing, fiber bundle and core are configured

such that liquid entering the liquid inlet passes through the fiber bundle and into the liquid outlet.

An alternative embodiment of the paracorporeal respiratory assist lung of the present invention includes a housing having a liquid inlet, a liquid outlet, a gas inlet and a gas outlet. The PRAL device includes a plurality of tubular gas permeable fiber membranes configured to form a fiber bundle, the fiber bundle being disposed within the housing and connected to and in fluid communication with the gas inlet and the gas outlet, wherein a first gap is configured between the housing and the fiber bundle. The device is configured with a core being disposed within the fiber bundle, wherein a second gap is configured between the core and the fiber bundle. The device may include a mechanism for rotating the core, wherein the housing, fiber bundle and core are configured such that liquid entering the liquid inlet passes through the fiber bundle and into the liquid outlet. The PRAL device may further be configured for creating turbulent flow within the second gap and creating a plurality of Taylor vortices within the second gap. In addition, the fiber bundle may be configured with a porosity that allows uniform liquid flow through the fiber bundle. Further, the PRAL device may be configured such that the first gap and the second gap are configured to optimize liquid flow through the fiber bundle.

Other features and advantages of the invention will become apparent from the following detailed description, taken in conjunction with the accompanying drawings, which illustrate, by way of example, the features of the invention.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 depicts placement in vivo of the paracorporeal respiratory assist lung of the present invention.

FIGS. 2A-2C depict several views of one embodiment of the paracorporeal respiratory assist lung of the present invention.

FIGS. 3A-3D depict several views of an alternative embodiment of the paracorporeal respiratory assist lung of the present invention.

FIGS. 4A and 4B are schematic representations of the paracorporeal respiratory assist lung of the present invention showing a rotating bundle.

FIGS. 5A-5P depict several views of an alternative embodiment of the paracorporeal respiratory assist lung of the present invention.

FIG. 6 depicts an alternative embodiment of the paracorporeal respiratory assist lung of the present invention.

FIG. 7 depicts an alternative embodiment of the paracorporeal respiratory assist lung of the present invention.

FIGS. 8A-8D depict several views of an alternative embodiment of the paracorporeal respiratory assist lung of the present invention.

FIG. 9 depicts schematic view of an alternative embodiment of the paracorporeal respiratory assist lung of the present invention having a magnetic drive mechanism.

FIGS. 10A and 10B depict an alternative embodiment of the paracorporeal respiratory assist lung of the present invention.

FIG. 11 is a cross-sectional view of the paracorporeal respiratory assist lung of FIG. 10.

FIGS. 12A and 12B are schematic representations of the paracorporeal respiratory assist lung of FIG. 11.

FIG. 13 depicts schematic view of an alternative embodiment of the paracorporeal respiratory assist lung of the present invention.

FIG. 14 is a block diagram of the system of the present invention.

FIG. 15 depicts a cross-sectional view of an alternative embodiment of the paracorporeal respiratory assist lung of the present invention having a magnetic drive mechanism.

FIGS. 16A and 16B are cage mechanism in accordance with the present invention for use with the fiber bundle.

FIGS. 17A, 17B depict schematic representations of a fiber mat having spacers for use in the paracorporeal respiratory assist lung of the present invention.

FIG. 18 is a block diagram in accordance with the system of the present invention.

FIG. 19 is a block diagram in accordance with the system of the present invention.

FIG. 20 is a graphical representation of gas exchange rates achieved with an embodiment of a paracorporeal respiratory assist lung of the present invention.

FIG. 21 is a graphical representation of gas exchange rates achieved with an embodiment of a paracorporeal respiratory assist lung of the present invention.

FIG. 22 is a graphical representation of blood flow (pumping) achieved with an embodiment of a paracorporeal respiratory assist lung of the present invention.

FIG. 23 is a graphical representation of a model prediction based on the porosity of the fiber bundle.

FIGS. 24 and 25 are graphical representations of carbon dioxide removal and blood flow (pumping) achieved with varied porosity of the fiber bundle in the paracorporeal respiratory assist lung of the present invention.

FIG. 26 is a graphical representation of the model (FEM-LAB) of blood flow through the fiber bundle.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

The present invention is directed to an improved veno-venous extracorporeal oxygenator, referred to herein as a “paracorporeal respiratory assist lung” or “PRAL device.” The paracorporeal respiratory assist lung of the present invention includes a rotating hollow fiber membrane bundle to increase the gas exchange efficiency of the device by reducing the boundary layer phenomena caused by blood flowing over the fibers. U.S. Pat. Nos. 5,830,370 (Maloney et al.); 5,900,142 (Maloney et al.); 6,106,776 (Borovetz et al.); 6,217,826 (Reeder et al.); 6,348,175 (Borovetz et al.); 6,723,284 (Reeder et al.) and U.S. Publication No. 2004/0219,061 (Reeder et al.) are incorporated herein in their entirety by reference.

The paracorporeal respiratory assist lung of the present invention has been developed for patients suffering from acute lung failures and acute exacerbations of chronic lung diseases. The design concept builds upon the clinical success of previous oxygenators that remove blood from the femoral artery of the patient, removes carbon dioxide (CO₂) via a commercially available membrane oxygenator and utilizes the natural arterio-venous pressure gradient to direct the blood to the femoral vein. The present invention uses an annular rotating hollow fiber membrane bundle to increase gas exchange and enable the device to pump blood. The increased gas exchange enables a lower surface area than current commercially available membrane lungs, and the pumping capacity of the rotating bundle enables blood flow through a percutaneous dual lumen cannula inserted exclusively on the venous circulation.

The main limitation to gas transfer in blood oxygenators is the diffusional boundary layer created by fluid flow along the surfaces of the fiber membranes. Effective movement of the fibers relative to the fluid (blood) can help reduce this boundary layer. In the invention described here, the hollow fibers of

the oxygenator are configured into an annular bundle that is rotated about a central axis. The placement of the hollow fibers in an annulus distinguishes this rotating oxygenator from known spinning disk rotating oxygenators. In such an annular configuration, the spinning of the fiber bundle provides a more uniform linear velocity to the fibers because all the fibers are at comparable distance from the axis of rotation. Accordingly, the paracorporeal respiratory assist lung of the present invention can achieve a given level of gas exchange at lower rotational speed than in spinning disk type oxygenators.

The paracorporeal respiratory assist lung of the present invention includes an outer housing that incases the fiber annulus, a motor connected to a shaft that spins the fiber annulus, and seals and bearings that separate the fluid and gas pathways. The proximal and distal manifolds may be configured with mechanisms, such as vanes, to aid in the mixing of fresh blood into the spinning fiber bundle. The fluid (blood/water) flows through a center pathway within the rotating shaft of the device that supports the fibers. With the rotation of this fluid pathway/fiber assembly, the fluid velocities that pass through the fibers and exchange gas can be regulated by controlling the rotational rate of the fiber bundle. With the fiber annulus of this device configured to a set distance from the center of rotation, more consistent velocities past the fibers are achieved, uniformly utilizing all the fibers, unlike a disc type oxygenator that generates various velocities along their surfaces.

The paracorporeal respiratory assist lung of the present invention has distinct advantages over current rotational technologies:

- rotating annular fiber bundle instead of a stationary fiber bundle;
- rotating fiber bundle in annular shape instead of disk (velocity does not go to zero near the axis of rotation);
- rotation can be steady/unsteady (time varying increases mass transfer and pumping at the mean steady value);
- annulus can be fabricated over a range of porosities (higher porosity leads to higher gas exchange without a significant effect on pumping);
- the annulus can be a thin bundle which leads to more shear penetration from the stationary walls surrounding the bundle;
- hemolysis is not due to the rotating fibers themselves (the device is configured using a porous stainless steel cage for support during rotation);
- various technologies have been developed to vary the fiber bundle porosity;
- rotation of the fiber bundle appears to make the flow paths more uniform so that gas exchange is not affected by the design or location of the inflow/outflow ports;
- pumping allows veno-venous percutaneous operation; and levels of CO₂ removal due to rotation of the fiber bundle may enable respiratory dialysis or low-flow CO₂ removal.

As shown in FIG. 1, a paracorporeal respiratory assist lung (PRAL device) is configured with a motor drive 28 for positioning outside of the body of a patient 25. The PRAL device includes a blood flow catheter 21 that may be inserted into the femoral vein 27 of the patient. Alternatively, the PRAL blood catheter may be inserted through the jugular vein 29 of the patient. The proximal end 45 of the PRAL blood catheter 21 may be inserted through a cut down 23 or percutaneous access in the leg of the patient for placement into the femoral vein. The catheter is guided through the patient’s vasculature to a position proximate the patient’s heart such that the distal end 45 is close to the heart, for example in or near the vena cava. The PRAL blood catheter may be configured with a dual

lumen having one side **47** for a blood inlet and a second side **46** for a blood outlet. It may be advantageous to notch the catheter distal end such that the blood outlet end **46** extends distal of the blood inlet opening **47**.

Referring now to FIGS. **2A**, **2B** and **2C**, one embodiment of the paracorporeal respiratory assist lung **20** of the present invention includes an outer housing **22** surrounding a stationary core **24**. A rotating fiber bundle **26** is contained within the outer housing and around the stationary core. A motor drive mechanism **28** is operably connected to the main housing of the paracorporeal respiratory assist lung. The stationary core includes a main body **30** having a blood inlet port **32** that allows blood to diffuse from the stationary core through a fiber mat **40** of the rotating fiber bundle. The outer housing is further configured with a blood outlet port **34** that, along with the blood inlet, may be connected to a cannula (not shown) configured to be inserted into the patient vasculature (FIG. **1**). The outer housing is further configured with a gas inlet nozzle **36** and a gas outlet nozzle **38** that are in fluid communication with the fiber mat of the rotating fiber bundle. The fiber mat is fixedly connected to a support mechanism **42** that is connected to a drive shaft **44** that is operably connected to the motor drive mechanism. The support mechanism for the fiber mat may be configured as a wire or mesh cage (FIGS. **16A**, **16B**) or other suitable embodiments to enhance blood flow through the fiber bundle while minimizing any damage to the blood components, e.g., limiting hemolysis.

Referring now to FIGS. **3A**, **3B**, **3C** and **3D**, the paracorporeal respiratory assist lung **50** of the present invention includes a central outer housing **52** having a blood outlet port **64**. A first end portion **54** of the outer housing includes a blood inlet port **62** and a gas inlet nozzle **66**. A second end portion **58** of the outer housing includes a gas outlet nozzle **68**. The first and second ends of the housing may be configured with threads or other mechanism to secure the ends of the housing to the central portion. A rotating fiber bundle mechanism **56** is configured to be disposed within the housing and includes a support mechanism (not shown) for retaining the fiber bundle while allowing blood to flow from the housing inlet through the fibers. The fiber bundle may be formed from an annular fiber mat **60** that is in fluid communication with the gas inlet and the gas outlet. The rotating fiber bundle mechanism further includes a drive shaft **74** that may be mechanically connected to a motor mechanism (not shown). The rotating fiber bundle mechanism may be further configured with a potting **72** to hold the ends of the fibers of the fiber mat.

Referring now to FIGS. **4A** and **4B**, the paracorporeal respiratory assist lung **80** used for testing purposes generally is configured with an outer housing **82** that surrounds a rotating fiber bundle **86** having a stationary core **84** disposed with the fiber bundle and the housing. Blood **100** enters the device through an inlet port **92** of the stationary core. Oxygen laden sweep gas **96** enters the rotating fiber core so that oxygen and carbon dioxide are exchanged to and from the blood along the fiber bundle. The rotating fiber bundle is configured with a drive shaft **104** for rotating the fiber bundle relative to the stationary core and outer housing. Referring to FIGS. **20**, **21** and **22**, typical experimental conditions using the paracorporeal respiratory assist lung of the present invention that achieved (a) increased CO₂ removal per area by 133%; (b) increased O₂ removal per area by 157%; and (c) generated 1 l/min flow against fifty mmHg at 1500 rpm include: (i) test fluid of water or slaughterhouse bovine blood; (ii) fluid flow rate at 750 ml/min; (iii) sweep gas flow rate at 6.5 l/min; (iv) loop temperature at 37° C.; (v) inlet pCO₂ at 45+/-5 mmHg;

(vi) inlet O₂ saturation at 65%; (vii) blood hematocrit at 35%; and (viii) blood hemoglobin concentration at 12.1 milligrams per deciliter (mg/dl).

A hollow fiber membrane bundle that has an annular cylindrical geometry can function as a pump when the bundle is rotated. Fluid in the bundle, however, becomes significantly entrained in the fiber rotational motion (the relative velocity between the fibers and the fluid goes to zero), and hence the rotation does not increase mass transfer efficiency for fiber bundles more than a few layers thick. A hollow fiber membrane bundle can be oscillated to reduce the entrainment of fluid because oscillation hinders the fluid velocity from reaching the fiber velocity. One aspect of the present invention is to introduce oscillations in the steady rotation of a hollow fiber bundle to increase the mass transfer efficiency of the device while maintaining its pumping capabilities.

As shown in FIGS. **18** and **19**, the paracorporeal respiratory assist lung of the present invention acts as an integrated pump/hollow fiber membrane mass transport device, and shows mass transfer enhancement when the rotational velocity of the fiber bundle is rapidly varied. To enhance performance of the gas exchange achieved by the paracorporeal respiratory assist lung, various modes of spinning the fiber bundle may be employed, e.g., steady rotation, unsteady rotation, purely oscillatory rotation and other forms of time-dependent rotation. As will be appreciated by those of ordinary skill in the art, known and to-be-developed gas-permeable fibers may be used with the present invention, for example, hollow microporous polypropylene fibers and gas-permeable fibers currently used in blood oxygenators. The gas-permeable fibers may include a coating of a gas-permeable polymer and may be bonded with a non-thrombogenic component.

The rotation actuator device may include a motor that is coupled to the fiber bundle. Oxygen is passed through the hollow fibers, and fluid (e.g., water or blood) may be introduced to the fiber bundle through an internal diffuser. Seals and bearings separate the gas and fluid pathways and allow the fiber bundle to be rotated with an external motor. A brushless DC servomotor may control the motion of the hollow fiber membrane bundle. The user of the paracorporeal respiratory assist lung may set the frequency and amplitude of oscillation with a computer connected to a controller. The controller signals a drive to perform the input motion while getting feedback from the motor and making adjustments to the velocity.

In a further embodiment of the present invention, the paracorporeal respiratory assist lung is configured to increase the porosity in the rotating fiber bundle. The increased porosity provides more fluid to flow through the fiber bundle, thus increasing the overall mass transfer efficiency of the device. The extra porosity in the fiber bundle is created by several possible ways including, but not limited to, using spacers to create void space between the fiber layers, removing every other fiber in the mat and using smaller diameter fibers. Additionally, support threads could be removed from the fiber fabric, and the paracorporeal respiratory assist lung could be configured such that the manifolds are relatively closer so as to "puff out" the fiber bundle.

As shown in FIGS. **17A** and **17B**, spacers can be created by placing thin strips of felt that are soaked in polyurethane or other suitable material across a fiber mat. In accordance with the present invention, as the fiber mat is rolled up, the felt is rolled with it, which then hardens as the adhesive dries. The dried felt then creates the extra space between the fibers. However, the fiber surface area where the felt is touching is not included in the operable surface area of the paracorporeal respiratory assist lung. Alternatively, by removing every other

fiber in the fiber mat, the fiber mat is left with many open spaces having only wefts and no fibers. The same overall surface area and number of fibers may be the same, but the fibers are much more spaced out, thus creating a “puffy bundle.” Further, gas-permeable fibers having a reduced outer diameter can also be used to create higher porosity devices. The higher porosity of the fiber bundle results from a reduced fiber density, i.e., the fiber density in a mat of smaller outer diameter fibers is less than fiber mats having larger outer diameter fibers. There is much more open space where only wefts exist, similar to configurations of the fiber bundle where every other fiber is removed.

The paracorporeal respiratory assist lung of the present invention achieves significant CO₂ removal (100-120 ml/min) at relatively low veno-venous blood flow rates (500-1000 ml/min) without the need for a separate pump. FIGS. 23-25 demonstrate the effect of fiber bundle porosity on the gas exchange and pumping performance of the paracorporeal respiratory assist lung. Two prototype paracorporeal respiratory assist lung devices were fabricated with bundle porosities of 0.43 and 0.83, but otherwise similar with membrane areas of 0.42 square meters (m²) and 0.50 m² respectively. The devices were tested for gas exchange in a flow loop using water as the test fluid at three l/min. The paracorporeal respiratory assist lung prototype with the higher bundle porosity achieved CO₂ removal at 1500 rpm of 173 ml/min/m² compared to 190 ml/min/m² for the prototype with the lower bundle porosity. In bovine blood, the paracorporeal respiratory assist lung with the higher bundle porosity at 1500 rpm achieved a CO₂ removal rate of 182 ml/min/m² at a blood flow rate of only 750 ml/min. In a separate pump test in water, the fiber bundle with higher porosity generated 67 mmHg compared to only 52 mmHg for the fiber bundle with the lower porosity at 0.75 l/min flow at 1500 RPM with water as the test fluid. The fiber bundle with increased porosity is within ten percent of a gas exchange target, and the pumping ability is consistent with generating 750 ml/min blood flow through percutaneous cannula less than 20 Fr.

Referring now to FIGS. 5A through 5P, one embodiment of the PRAL device includes an outer housing 520 having an upper portion 524 and a lower portion 522. The upper portion of the PRAL device 500 includes a blood inlet 530 and a gas outlet 545. The lower portion of the housing includes a gas inlet 540 and a blood outlet port 535. This embodiment of the PRAL device includes a rotating fiber bundle having an external drive connection 525. As shown in FIG. 5D, the drive mechanism 525 is connected to an internal coupling 527 that can exit to the fiber bundle 550. The PRAL device includes a stationary core 560 that is configured with a lumen or blood conduit having an outside end 532 and an inside end 534. The inside end of the blood conduit is attached to an impeller device 570 which may include a plurality of arcuate arms 572 that assist in directing blood flow through the fiber bundle 550. The PRAL device is configured with an annular space 590 between the rotating fiber bundle 550 and the outer housing 520. Blood flow commencing at the entrance 530 and traveling from the impeller 570 through the fiber bundle 550 and gap 590 exits through the port 535. Sweep gas, such as oxygenated air, enters the PRAL device through entry port 540 travels through the fiber bundle 550 wherein carbon dioxide and oxygen are exchanged with the blood and the carbon dioxide laden gas exits through the port 545 in the upper portion 524 of the PRAL device. The upper portion of the PRAL device is further configured with a retaining device 565 that secures the core 560 and blood conduit 530 within the housing 520.

Referring now to FIG. 6, an alternative embodiment of the PRAL device 600 includes an outer casing 620 having a blood and fluid inlet 630 and fluid outlet 635 passes through the inlet through a conduit 632 that bifurcates into a first conduit 634 and a second conduit 636 that direct blood through the fiber bundle 650. The fiber bundle is connected to a drive mechanism 625 that is connected to a motor drive 628. A plurality of sealing mechanisms 690 are included to separate the rotating fiber bundle and blood flow from the gas pathway. Gas enters the system through inlet 640 that is connected to the fiber bundle and exits through the gas outlet port 645 in fluid communication with the fiber bundle 650.

Referring now to FIG. 7, an alternative embodiment of the PRAL device 700 includes an outer casing 720 having a blood and fluid inlet 730 and fluid outlet 735 passes through the inlet through a conduit 732 that directs blood through the fiber bundle 750. The fiber bundle is connected to a drive mechanism 725 that is connected to a motor drive 728. A plurality of sealing mechanisms 790 are included to separate the rotating fiber bundle and blood flow from the gas pathway. Gas enters the system through inlet 740 that is connected to the fiber bundle and exits through the gas outlet port 745 in fluid communication with the fiber bundle 750. This particular embodiment further includes a stationary core 760 positioned inside of the rotating fiber bundle 750.

Referring now to FIG. 8 is an alternative embodiment of the PRAL device 800 in accordance with the present invention. The PRAL device includes an outer shell 820 having a lower portion 822 and an upper portion 824 secured to the main body 820. The upper portion of the device includes a blood inlet 830 connected to a conduit 832 having a distal end 834 for providing blood flow through a central core 860 and an impeller 870. The blood flow passes through a rotating fiber bundle 850 that is connected to a drive mechanism 825. Gas enters from the lower portion 822 of the housing through an inlet gas port 540 that is in fluid communication with the fiber gas bundle 850 and an exit gas port 845. A small annular gap 890 resides between the rotating fiber bundle 850 and the outer housing 820 of the device 800. Various seals and other mechanisms are used to isolate the gas flow from the blood flow. Similarly, screws and other mechanisms are used to secure the portions of the housing. In addition various seals and bearings are used to allow the drive mechanism and rotating core to freely move within the housing.

Referring now to FIG. 9, an alternative embodiment of the PRAL device 900 in accordance with the present invention includes magnetic couplings for rotating a central core. The PRAL device includes a housing 920 having a lower portion 922 and an upper portion 924. The upper portion includes a blood inlet conduit 930 that is connected to a blood distribution impeller 970 embodied within the rotating core 960. The lower portion of the body 922 includes seals and bearings 980 and a pin or other mechanism 982 for the rotating core to rest within the housing. This embodiment of the PRAL device includes a stationary fiber bundle 950 having a gas inlet 940 and a gas outlet 945. Blood flows from the inlet 930 through an internal gap 922 past the bundles 950 through a recirculation gap 990 and out the blood exit port 935. The internal and recirculation gaps between the rotating core and the outer housing allow for a recirculation or eddy effect shown by arrows 996. The rotating core is magnetically coupled to an external device via magnets 984 and 986 secured to the rotating core.

Referring now to FIGS. 10A and 10B, an alternative embodiment of the PRAL device 1000 may be further configured with a rotating core mechanism. The PRAL device includes an outer body 1020 having a lower portion 1022 and

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an upper portion **1024**. A motor drive mechanism **1025** is configured within the lower portion. A gas inlet port **1040** is also configured in the lower portion of the housing. A stationary fiber bundle **1050** is positioned within the main body **1020** of the housing that is configured to accept a rotating cord **1060**. Various seals and securing devices **1062**, **1064**, **1066** and **1068** are shown in FIG. 10B.

Referring now to FIG. 11, the PRAL device **1100** is also configured with a rotating core mechanism and stationary fiber bundle. The device is configured with an outer housing **1120** having a lower portion **1122** and an upper portion **1124** that are secured together forming a single unit. The lower portion of the housing includes a motor drive mechanism **1125** operably secured to a rotating core **1160**. Blood enters from a top portion of the unit through a blood entry port **1130** and travels to an impeller **1170**. Blood flows from the impeller through an internal gap **1192** past the stationary fiber bundle **1150** through an outer recirculation gap **1190** and through an exit blood port (not shown). Gas enters the fiber bundle through an entry port **1140** and exits after passing through the fiber bundle through an exit port **1145** configured at the top of the PRAL device. The gas entry port is located in the lower portion **1122** of the PRAL housing **1120**. A stabilizing portion **1180** secured to the lower portion of the housing includes bearings and seals configured to accept the rotating drive mechanism **1125**. Other various seals and bearings may be employed to separate gas and blood flow and to prevent leakage of the fluids.

Referring now to FIGS. 12A and 12B, top and bottom views in partial cutaway are shown regarding the PRAL device of FIGS. 10 and 11. As shown in FIG. 12A, blood flow is directed into impeller **1170** having a plurality of arcuate flow directing arms **1172**. The blood flow continues from the impeller to an internal gap **1192** disposed between the rotating core **1160** and stationary fiber bundle **1150**. The blood flow travels through the stationary fiber bundle to an outer recirculation gap **1192** and out through the blood exit port **1135**.

FIG. 26 is a FEMLAB CFD (computational fluid dynamics) simulation of blood flow occurring in one embodiment of the PRAL device of the present invention. Shown is the longitudinal cross-section of the FEMLAB model for the case of a PRAL device with a rotating fiber bundle **2650** positioned between a stationary inner housing **2600** and a stationary outer housing **2700**. A first outer gap **2690** is formed between the outer housing **2700** and the fiber bundle **2650**, and a second inner gap **2692** is formed between the inner housing **2600** and the fiber bundle **2650**. Rotation of the annular fiber bundle **2650** creates Taylor vortices **2635** in the outer gap **2690** between the rotating fiber bundle **2650** and the stationary outer housing **2700**. The vortices **2635** create pressure variations **2630** in the outer gap **2690**. The pressure variations disturb the blood flow pattern **2620** within the fiber bundle **2650**, augmenting relative velocity between the rotating fibers and the blood, thereby improving gas exchange. In this and other embodiments of the PRAL device, the size of the outer gap **2690** between the annular fiber bundle **2650** (rotating or stationary) and the outer housing **2700** has a preferred size range. The gap size should be just large enough that the pressure drop encountered by blood traversing the outer gap **2690** to the device outlet be configured so as to not prevent the establishment of a relatively uniform distribution of radial blood flow through the annular fiber bundle **2650**. This gap size will be conditional on the permeability (porosity) and thickness of the fiber bundle.

Referring now to FIG. 13, an alternative embodiment of the PRAL device of the present invention includes a bundle of

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fibers configured with the rotating core in addition to a stationary fiber bundle. The PRAL device includes a housing **1320** having a lower portion **1322** and an upper portion **1324**. The upper portion includes a blood inlet conduit **1330** that is connected to a blood distribution impeller **1370** embodied within the rotating core **1360**. The lower portion of the body **1322** includes seals and bearings **1380** and a pin or other mechanism **1382** for the rotating core to rest within the housing. This embodiment of the PRAL device includes a stationary fiber bundle **1350** having a gas inlet **1340** and a gas outlet **1345**. Blood flows from the inlet **1330** through an internal gap **1322** past the bundles **1350** through a recirculation gap **1390** and out the blood exit port **1335**. The internal and recirculation gaps between the rotating core and the outer housing allow for a recirculation or eddy effect. The rotating core is magnetically coupled to an external device via magnets **1384** and **1386** secured to the rotating core. Additional conduit **1385** is included for providing gas flow into and out of the rotating fiber bundle **1355**.

Referring now to FIG. 14, a block diagram is shown depicting the PRAL device **1400** configured with control in electronics computer system **1410** having a user interface **1420** with battery pack and charger **1430** and AC-DC power supply **1435**. The system may be further configured with Ethernet or other external communication devices **1425**, **1427**. Blood enters the PRAL device through inlet line **1430** and exits to the patient through outlet port **1435** having safety mechanisms such as flow and bubble detectors. An air inlet **1440** is supplied and may be connected to a wall oxygen supply unit **1442** or oxygen tank **1444** for supplementing gas to the device. A humidifier and/or heater **1475** may be interposed between the air inlet and the PRAL device **1400**. The sweep gas exhaust line **1445** may include a water trap **1446** and carbon dioxide and oxygen analyzers **1448**. Other valves and venting mechanisms may be included for safety devices. For example, a vacuum pump **1490** may be interposed between the PRAL device **1400** and the exit ports **1495** to create a safety mechanism so that the system has a negative pressure so as to not create bubbles within the patient's vasculature.

FIG. 15 depicts an alternative embodiment of the PRAL device of the present invention. The PRAL device **1500** is also configured with a rotating core mechanism and stationary fiber bundle. The device is configured with an outer housing **1520** having a lower portion **1522** and an upper portion **1524** that are secured together forming a single unit. The lower portion of the housing includes a drive mechanism **1580**, **1582** operably secured to a rotating core **1560**. Blood enters from a top portion of the unit through a blood entry port **1530** and travels to an impeller **1570** having a plurality of arms **1572**. Blood flows from the impeller through an internal gap **1592** past the stationary fiber bundle **1550** through an outer recirculation gap **1590** and through an exit blood port (not shown). Gas enters the fiber bundle through an entry port (not shown) and exits after passing through the fiber bundle through an exit port (not shown) configured at the top of the PRAL device. The gas entry port is located in the lower portion **1122** of the PRAL housing **1120**. The device includes magnets **1584** and **1586** for coupling to an external drive mechanism. Other various seals and bearings may be employed to separate gas and blood flow and to prevent leakage of the fluids. The magnets and housing may be configured to allow the rotating core to levitate above the bottom portion of the housing, thereby reducing friction in the device. Other various seals and bearings may be employed to separate gas and blood flow and to prevent leakage of the fluids.

While particular forms of the invention have been illustrated and described, it will also be apparent to those skilled in

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the art that various modifications can be made without departing from the inventive concept. References to use of the invention with a membrane electrode assembly and fuel cell are by way of example only, and the described embodiments are to be considered in all respects only as illustrative and not restrictive. The present invention may be embodied in other specific forms without departing from its spirit or essential characteristics. Accordingly, it is not intended that the invention be limited except by the appended claims.

We claim:

1. A paracorporeal respiratory assist lung, comprising:
 - a housing having a smooth inner cylindrical surface, a liquid inlet, a liquid outlet, a gas inlet and a gas outlet;
 - a plurality of tubular gas permeable fiber membranes configured to form a cylindrical annular fiber bundle, the annular fiber bundle being disposed within the housing and connected to and in fluid communication with the gas inlet and the gas outlet wherein gas is passed through the lumens of the cylindrical annular fiber bundle, wherein a first annular gap is configured between the housing and the fiber bundle;
 - a stationary cylindrical core with a smooth outer surface being positioned concentrically within the annular fiber bundle, wherein a second annular gap is configured between the smooth outer surface the core and the annular fiber bundle; a stationary cylindrical core with a smooth outer surface being positioned concentrically within the annular fiber bundle, wherein a second annular gap is configured between the smooth outer surface of the core and the fibers of the annular fiber bundle; an impeller having the same diameter as the core and in fluid communication with the liquid inlet via a conduit within the core, the impeller fixed to the interior of a lower portion of the annular fiber bundle; the impeller comprised of a plurality of arcuate arms each culminating in an exit port aligned with the smooth outer surface

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of the stationary core and ending in the lower portion of the second annular gap; and
 means for rotating the annular fiber bundle and fixed impeller, wherein rotating the annular fiber bundle cooperates with the smooth inner surface of the housing and the first annular gap to create and maximize Taylor vortices within the first annular gap; and
 wherein the housing, annular fiber bundle and core are configured such that liquid traveling at a low flow rate enters the liquid inlet, travels down the conduit through the impeller which pumps the liquid in to the second annular gap and radially through the tubular gas permeable hollow fiber membrane, having the Taylor vortices cause the liquid to pass the back and forth through the fiber bundle and the annular gaps to maximize gas exchange, the liquid eventually exiting through the liquid outlet.

2. The paracorporeal respiratory assist lung of claim 1, wherein the fiber bundle is configured with a porosity that allows uniform liquid flow through the fiber bundle; said porosity is determined by the diameter of the hollow fiber membrane and by arrangement and spacing between hollow fiber membranes.
3. The paracorporeal respiratory assist lung of claim 1, further comprising means for varying a velocity of the rotation of the fiber bundle.
4. The paracorporeal respiratory assist lung of claim 1, further comprising means for oscillating a direction of the rotation of the fiber bundle.
5. The paracorporeal respiratory assist lung of claim 1, further comprising a dual lumen cannula configured for insertion into the venous circulation of a patient to provide blood flow to the liquid inlet of the housing and to accept blood flow from the liquid outlet of the housing.

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